

### 6.3 Example Problem 3 - Movable Bed

The following example demonstrates how to add sediment data to the previously developed file. Existence of sediment data within the input file causes HEC-6 to compute sediment transport rates and modify the cross section geometry as described in Section 2.3. Sediment related data consists of the delineation of the movable bed, characteristics and gradation of sediment within the bed, and inflowing/outflowing sediment loads and gradations. The sediment data is inserted between the EJ record of the geometry data and the SHYD record of the flow data. Table 6-3a shows the input data developed for Example Problem 3.

#### 6.3.1 Movable Bed Limits

Information delineating the movable bed have been added to the HD record of each cross section. For example, at Section No. 1.0, the movable bed limits have been defined at stations 10,081 and 10,250. The "fixed" GR points are those outside of the movable bed stations; that is, should a limit of the movable bed coincide with a GR point, that point is movable and the next point outward is fixed.

The vertical limit (initial depth) of the movable portion of the cross section must also be defined. Data describing the location of this bedrock is entered in Field 2 of the HD record for each cross section. In Example Problem 3, it was determined that the reach represented by Section No. 58.0 had bedrock 3.4 ft below the thalweg. Section No. 33.0 through Section No. 42.1 have either concrete or bedrock at the thalweg.

#### 6.3.2 Sediment Title Records

Five title records (T4-T8) are required at the beginning of the sediment data; these records are available for user documentation of the sediment data.

#### 6.3.3 Sediment Transport Control Parameters

Parameters governing the computation of sediment transport rates and selection of grain sizes are entered on the I records. For Example Problem 3, the number of times that the bed material gradation is to be re-calculated within a time step is set to 5 on the I1 record (see Section 2.3.1.4). Default values for the other parameters on this record will be used. Only sands and gravels are analyzed in Example Problem 3. Since there are no clays or silts in either the bed or the inflowing load, there are no I2 or I3 records. Ten sand and gravel sizes are being analyzed as seen by the 1 in Field 3 and 10 in Field 4 of the I4 record. The transport computation method chosen is that of Yang (4 in Field 2 of the I4 record). Default values for the other parameters were selected, by not providing data. It is important to remember that the range of grain sizes selected on the I records must encompass the entire range of sizes found in both the bed material and inflowing load, even though some of those sizes may be missing in either the bed or inflowing materials.

The "most stable" weighting scheme for the hydraulic parameters has been selected via the I5 record (see Section 2.2.4).

---

---

---

|          |   |        |        |        |        |        |        |        |        |
|----------|---|--------|--------|--------|--------|--------|--------|--------|--------|
| GR 1000. | 980.  | 990.0  | 1060.  | 980.0  | 1150.  | 982.00 | 1180.  | 982.0  | 1215.  |
| GR 980.0 | 1260.   | 982.0  | 1300.  | 982.0  | 1350.  | 980.00 | 1420.  | 980.0  | 1540.  |
| GR 982.0 | 1730.   | 982.0  | 1830.  | 984.41 | 1850.  | 979.19 | 1851.  | 961.0  | 1900.8 |
| GR 961.0 | 2099.2  | 976.0  | 2149.  | 984.5  | 2150.  | 982.00 | 2800.  | 990.0  | 3100.  |
| GR 1000. | 3170.   |        |        |        |        |        |        |        |        |
| HD 33.0  | 0.  | 1851.  | 2149.  |        |        |        |        |        |        |
| NOTE:    | Section 33.3 is a duplicate of Section 33.0.  |        |        |        |        |        |        |        |        |
|          | Section 33.0 is a good representative cross section for a long reach. A duplicate is used here to break up the long reach into two smaller reaches. |        |        |        |        |        |        |        |        |
| X1 33.3  | 21  | 1850.  | 2150.  | 1550.  | 1750.  | 1750   | .95    | 1.49   |        |
| XL       |   | 250.   |        |        |        |        |        |        |        |
| GR 1000. | 980.  | 990.0  | 1060.  | 980.0  | 1150.  | 982.00 | 1180.  | 982.0  | 1215.  |
| GR 980.0 | 1260.   | 982.0  | 1300.  | 982.0  | 1350.  | 980.00 | 1420.  | 980.0  | 1540.  |
| GR 982.0 | 1730.   | 982.0  | 1830.  | 984.41 | 1850.  | 979.19 | 1851.  | 961.0  | 1900.8 |
| GR 961.0 | 2099.2  | 976.0  | 2149.  | 984.5  | 2150.  | 982.00 | 2800.  | 990.0  | 3100.  |
| GR 1000. | 3170.   |        |        |        |        |        |        |        |        |
| HD 33.3  | 0.  | 1851.  | 2149.  |        |        |        |        |        |        |
|          | Section 33.9 is a duplicate of Sec 33.3, needed to model IBC at Sec 35.0  |        |        |        |        |        |        |        |        |
| X1 33.9  | 21  | 1850.  | 2150.  | 1050.  | 1050.  | 1050.  | .95    | 1.65   |        |
| X3 10    |   |        |        |        |        |        |        |        |        |
| GR 1000. | 980.  | 990.0  | 1060.  | 980.0  | 1150.  | 982.00 | 1180.  | 982.0  | 1215.  |
| GR 980.0 | 1260.   | 982.0  | 1300.  | 982.0  | 1350.  | 980.00 | 1420.  | 980.0  | 1540.  |
| GR 982.0 | 1730.   | 982.0  | 1830.  | 984.41 | 1850.  | 979.19 | 1851.  | 961.0  | 1900.8 |
| GR 961.0 | 2099.2  | 976.0  | 2149.  | 984.5  | 2150.  | 982.00 | 2800.  | 990.0  | 3100.  |
| GR 1000. | 3170.   |        |        |        |        |        |        |        |        |
| HD 33.9  | 0.  | 1851.  | 2149.  |        |        |        |        |        |        |
|          | A weir is located here.   |        |        |        |        |        |        |        |        |
| X1 35.0  | 22  | 9894.  | 10245. | 0      | 0      | 0      |        |        |        |
| X3 10    |   |        |        |        |        |        |        |        |        |
| X5       | 974.  | 0.5    |        |        |        |        |        |        |        |
| GR 984.0 | 9035.   | 980.0  | 9070.  | 978.0  | 9135.  | 980.00 | 9185.  | 982.0  | 9270.  |
| GR 980.0 | 9465.   | 981.7  | 9595.  | 983.7  | 9745.  | 984.70 | 9894.  | 963.4  | 9894.1 |
| GR 963.3 | 9954.   | 967.1  | 9974.  | 967.4  | 10004. | 968.20 | 10044. | 967.6  | 10054. |
| GR 973.4 | 10115.  | 977.4  | 10120. | 983.7  | 10155. | 984.00 | 10245. | 982.0  | 10695. |
| GR 982.0 | 10895.  | 1004.0 | 11085. |        |        |        |        |        |        |
| HD 35.0  | 0.  | 9954.  | 10155. |        |        |        |        |        |        |
| - - -    | Silver Lake - - -   |        |        |        |        |        |        |        |        |
| NC .06   | .06   | .045   |        |        |        |        |        |        |        |
| X1 42.0  | 32  | 9880.  | 10130. | 5370.  | 5000.  | 5210.  |        |        |        |
| GR 996.0 | 7130.   | 998.0  | 7310.  | 998.0  | 7930.  | 992.00 | 8205.  | 990.0  | 8495.  |
| GR 988.0 | 8780.   | 986.0  | 8990.  | 985.7  | 9570.  | 986.45 | 9707.  | 989.44 | 9857.  |
| GR 990.0 | 9880.   | 969.8  | 9881.  | 969.8  | 9941.  | 985.80 | 9941.  | 985.8  | 9943.  |
| GR 969.8 | 9943.   | 969.8  | 10001. | 986.7  | 10001. | 986.70 | 10003. | 969.8  | 10003. |
| GR 969.8 | 10067.  | 985.8  | 10067. | 985.8  | 10069. | 969.80 | 10069. | 969.8  | 10129. |
| GR 989.9 | 10130.  | 989.5  | 10180. | 988.6  | 10230. | 987.60 | 10280. | 985.2  | 10430. |
| GR 986.8 | 11720.  | 989.9  | 12310. |        |        |        |        |        |        |
| HD 42.0  | 0.  | 9881.  | 10021. |        |        |        |        |        |        |
|          | Silver Creek - local inflow   |        |        |        |        |        |        |        |        |
| QT       |   |        |        |        |        |        |        |        |        |
| X1 44.0  | 28  | 9845.  | 10127. | 3200.  | 3800.  | 3500.  |        |        |        |
| XL       |   | 9850.  | 10200. |        |        |        |        |        |        |
| GR 1002. | 8035.   | 992.0  | 8150.  | 990.0  | 8305.  | 990.00 | 8735.  | 988.0  | 8835.  |
| GR 996.0 | 9285.   | 1017.6 | 9425.  | 990.0  | 9505.  | 986.00 | 9650.  | 984.1  | 9788.  |
| GR 980.6 | 9845.   | 970.9  | 9868.  | 972.2  | 9898.  | 970.50 | 9968.  | 967.5  | 9998.  |
| GR 968.9 | 10028.  | 967.4  | 10058. | 967.1  | 10078. | 971.90 | 10118. | 976.8  | 10127. |
| GR 977.8 | 10150.  | 976.9  | 10193. | 982.0  | 10206. | 981.20 | 10300. | 979.2  | 10325. |
| GR 983.1 | 10400.  | 999.8  | 10450. | 1002.4 | 10464. |        |        |        |        |
| HD 44.0  | 1.  | 9868.  | 10193. |        |        |        |        |        |        |
| X1 53.0  | 22  | 10000. | 10136. | 3366.  | 2832.  | 2942.  |        |        |        |
| GR 1004. | 7550.   | 1000.0 | 7760.  | 998.0  | 8440.  | 996.00 | 8640.  | 996.0  | 8780.  |
| GR 994.0 | 8940.   | 986.0  | 9245.  | 986.3  | 9555.  | 986.30 | 9825.  | 983.8  | 9900.  |
| GR 982.8 | 10000.  | 978.2  | 10011. | 974.0  | 10041. | 972.20 | 10071. | 972.6  | 10101. |
| GR 978.2 | 10121.  | 988.7  | 10136. | 989.3  | 10154. | 999.20 | 10200. | 1000.1 | 10320. |
| GR 1002. | 10470.  | 1004.0 | 10700. |        |        |        |        |        |        |
| HD 53.0  | 10.   | 10000. | 10136. |        |        |        |        |        |        |
|          | Bear Creek - local inflow   |        |        |        |        |        |        |        |        |
| QT       |   |        |        |        |        |        |        |        |        |
| X1 55.0  | 18  | 9931.  | 10062. | 2275.  | 3430.  | 2770.  |        |        |        |
| GR 1004. | 7592.   | 1000.0 | 7947.  | 996.0  | 8627.  | 990.00 | 9052.  | 986.0  | 9337.  |
| GR 984.3 | 9737.   | 984.7  | 9837.  | 985.5  | 9910.  | 987.20 | 9931.  | 978.1  | 9955.  |
| GR 974.8 | 9975.   | 974.2  | 10005. | 972.9  | 10035. | 973.20 | 10045. | 983.8  | 10062. |
| GR 985.8 | 10187.  | 986.0  | 10307. | 990.0  | 10497. |        |        |        |        |
| HD 55.0  | 10.   | 9931.  | 10062. |        |        |        |        |        |        |
| X1 58.0  | 22  | 9912.  | 10015. | 1098.  | 1012.  | 1462.  |        |        |        |
| GR 1006. | 8542.   | 1004.0 | 8952.  | 1000.0 | 9702.  | 997.20 | 9812.  | 996.3  | 9912.  |
| GR 976.2 | 9944.   | 975.4  | 9974.  | 978.2  | 9991.  | 990.40 | 10015. | 988.3  | 10062. |
| GR 988.8 | 10065.  | 988.3  | 10065. | 989.3  | 10169. | 990.00 | 10172. | 992.0  | 10242. |
| GR 992.0 | 10492.  | 988.0  | 10642. | 986.7  | 10852. | 988.00 | 11022. | 986.0  | 11097. |
| GR 986.0 | 11137.  | 988.0  | 11192. |        |        |        |        |        |        |
| HD 58.0  | 3.4   | 9912.  | 10015. |        |        |        |        |        |        |
| EJ       |   |        |        |        |        |        |        |        |        |
| T4       | South Fork, Zumbro River - Stream Segment 1 ** Example Problem 3 **   |        |        |        |        |        |        |        |        |
| T5       | LOAD CURVE FROM GAGE DATA.  |        |        |        |        |        |        |        |        |
| T6       | BED GRADATIONS FROM FIELD SAMPLES.  |        |        |        |        |        |        |        |        |

|   |  |   |       |       |       |        |      |      |      |      |
|---|--|---|-------|-------|-------|--------|------|------|------|------|
| T7  | Use Full Range of Sands and Gravels                                      |   |       |       |       |        |      |      |      |      |
| T8  | SEDIMENT TRANSPORT BY Yang's STREAM POWER [ref ASCE JOURNAL (YANG 1971)] |   |       |       |       |        |      |      |      |      |
| I1  | 5  |   |       |       |       |        |      |      |      |      |
| I4  | SAND   | 4                                       | 1     | 10    |       |        |      |      |      |      |
| I5  |  | .5                                      | .5    | .25   | .5    | .25    | 0    | 1.0  |      |      |
| LQ  |  | 1                                       | 50    | 1000  | 5800  | 90000  |      |      |      |      |
| LT  | TOTAL  | .0110                                   | 1.5   | 320   | 4500. | 400000 |      |      |      |      |
| LF  | VFS  | .119                                    | .119  | .498  | .511  | .582   |      |      |      |      |
| LF  | FS   | .328                                    | .328  | .331  | .306  | .280   |      |      |      |      |
| LF  | MS   | .553                                    | .553  | .156  | .154  | .110   |      |      |      |      |
| LF  | CS   | .000                                    | .000  | .011  | .016  | .020   |      |      |      |      |
| LF  | VCS  | .000                                    | .000  | .004  | .008  | .005   |      |      |      |      |
| LF  | VFG  | .000                                    | .000  | .000  | .004  | .002   |      |      |      |      |
| LF  | FG   | .000                                    | .000  | .000  | .001  | .001   |      |      |      |      |
| LF  | MG   | .000                                    | .000  | .000  | .000  | .000   |      |      |      |      |
| LF  | CG   | .000                                    | .000  | .000  | .000  | .000   |      |      |      |      |
| LF  | VCG  | .0                                      | .0    | .000  | .000  | .000   |      |      |      |      |
| PF  | EXAMP  | 1.0                                     | 1.0   | 32.0  | 16.0  | 96.5   | 8.0  | 95.0 | 4.0  | 91.0 |
| PFC   | 2.0  | 85.0                                    | 1.0   | 73.0  | .5    | 37.0   | .25  | 8.0  | .125 | 1.0  |
| PFC   | .0625  | 0.0                                     |       |       |       |        |      |      |      |      |
| PF  | EXAMP  | 32.0                                    | 1.0   | 64.0  | 32.0  | 99.5   | 16.0 | 99.0 | 8.0  | 98.5 |
| PFC   | 4.0  | 96.0                                    | 2.0   | 93.5  | 1.0   | 83.0   | .50  | 45.5 | .250 | 8.0  |
| PFC   | .125   | 1.0                                     | .0625 | 0.0   |       |        |      |      |      |      |
| PF  | EXAMP  | 58.0                                    | 1.0   | 64.0  | 32.0  | 97.0   | 16.0 | 94.0 | 8.0  | 94.0 |
| PFC   | 4.0  | 90.0                                    | 2.0   | 79.0  | 1.0   | 56.0   | .50  | 4.0  | .125 | 0.0  |
| SLOCAL                                      |  |   |       |       |       |        |      |      |      |      |
| LOAD TABLE - CASCADE CREEK - A LOCAL INFLOW |  |   |       |       |       |        |      |      |      |      |
| LQL   |  | 1                                       | 100   | 1000  | 10000 |        |      |      |      |      |
| LTL   | TOTAL  | .0040                                   | 10    | 500   | 30000 |        |      |      |      |      |
| LFL   | VFS  | .664                                    | .664  | .015  | .198  |        |      |      |      |      |
| LFL   | FS   | .207                                    | .207  | .245  | .181  |        |      |      |      |      |
| LFL   | MS   | .086                                    | .086  | .605  | .107  |        |      |      |      |      |
| LFL   | CS   | .031                                    | .031  | .052  | .098  |        |      |      |      |      |
| LFL   | VCS  | .008                                    | .008  | .039  | .127  |        |      |      |      |      |
| LFL   | VFG  | .0030                                   | .0030 | .0200 | .1160 |        |      |      |      |      |
| LFL   | FG   | .0010                                   | .0010 | .0110 | .0910 |        |      |      |      |      |
| LFL   | MG   | .0000                                   | .0000 | .0110 | .0530 |        |      |      |      |      |
| LFL   | CG   | .0000                                   | .0000 | .0000 | .0220 |        |      |      |      |      |
| LFL   | VCG  | .0000                                   | .0000 | .0000 | .0060 |        |      |      |      |      |
| LOAD TABLE - SILVER CREEK - A LOCAL INFLOW  |  |   |       |       |       |        |      |      |      |      |
| LQL   |  | 1                                       | 100   | 1000  | 10000 |        |      |      |      |      |
| LTL   | TOTAL  | .0040                                   | 10    | 500   | 30000 |        |      |      |      |      |
| LFL   | VFS  | .664                                    | .664  | .015  | .198  |        |      |      |      |      |
| LFL   | FS   | .207                                    | .207  | .245  | .181  |        |      |      |      |      |
| LFL   | MS   | .086                                    | .086  | .605  | .107  |        |      |      |      |      |
| LFL   | CS   | .031                                    | .031  | .052  | .098  |        |      |      |      |      |
| LFL   | VCS  | .008                                    | .008  | .039  | .127  |        |      |      |      |      |
| LFL   | VFG  | .0030                                   | .0030 | .0200 | .1160 |        |      |      |      |      |
| LFL   | FG   | .0010                                   | .0010 | .0110 | .0910 |        |      |      |      |      |
| LFL   | MG   | .0000                                   | .0000 | .0110 | .0530 |        |      |      |      |      |
| LFL   | CG   | .0000                                   | .0000 | .0000 | .0220 |        |      |      |      |      |
| LFL   | VCG  | .0000                                   | .0000 | .0000 | .0060 |        |      |      |      |      |
| LOAD TABLE - BEAR CREEK - A LOCAL INFLOW    |  |   |       |       |       |        |      |      |      |      |
| LQL   |  | 1.                                      | 100.  | 500.  | 1000. | 30000. |      |      |      |      |
| LTL   | TOTAL  | .0020                                   | 30.0  | 500.  | 1200  | 22500  |      |      |      |      |
| LFL   | VFS  | .201                                    | .201  | .078  | .078  | .137   |      |      |      |      |
| LFL   | FS   | .342                                    | .342  | .172  | .175  | .218   |      |      |      |      |
| LFL   | MS   | .451                                    | .451  | .454  | .601  | .476   |      |      |      |      |
| LFL   | CS   | .001                                    | .001  | .197  | .142  | .158   |      |      |      |      |
| LFL   | VCS  | .000                                    | .000  | .000  | .003  | .008   |      |      |      |      |
| LFL   | VFG  | .0000                                   | .0000 | .0000 | .0000 | .0020  |      |      |      |      |
| LFL   | FG   | .0000                                   | .000  | .0000 | .0000 | .0010  |      |      |      |      |
| LFL   | MG   | .0000                                   | .000  | .0000 | .0000 | .0000  |      |      |      |      |
| LFL   | CG   | .0000                                   | .000  | .0000 | .0000 | .0000  |      |      |      |      |
| LFL   | VCG  | .0000                                   | .000  | .0000 | .0000 | .0000  |      |      |      |      |
| SHYD  |  |   |       |       |       |        |      |      |      |      |
| Q   | A  | FLOW 1 = BASE FLOW OF 750 CFS           |       |       |       |        |      |      |      |      |
| Q   | 750.   | 61.                                     | 29.   | 128.  |       |        |      |      |      |      |
| R   | 956.   | 962.                                    |       |       |       |        |      |      |      |      |
| T   | 65.  | 72.                                     | 70.   | 67.   |       |        |      |      |      |      |
| W   | 2.   |   |       |       |       |        |      |      |      |      |
| Q   | B  | FLOW 2 = 50 DAYS AT BANK FULL DISCHARGE |       |       |       |        |      |      |      |      |
| Q   | 2500.  | 300.                                    | 150.  | 650.  |       |        |      |      |      |      |
| R   | 965.   | 970.                                    |       |       |       |        |      |      |      |      |
| W   | 50.  |   |       |       |       |        |      |      |      |      |
| SPRT  |  |   |       |       |       |        |      |      |      |      |
| CP  |  | 1                                       |       |       |       |        |      |      |      |      |
| PS  |  | 15.0                                    | 32.0  | 32.1  |       |        |      |      |      |      |
| END   |  |   |       |       |       |        |      |      |      |      |
| Q   | AC   | FLOW 3 = NEAR BANK FULL DISCHARGE       |       |       |       |        |      |      |      |      |
| Q   | 1250.  | 150.                                    | 78.   | 340.  |       |        |      |      |      |      |
| R   | 960.   | 966.                                    |       |       |       |        |      |      |      |      |
| W   | 1.   |   |       |       |       |        |      |      |      |      |
| SPRT  | A  |   |       |       |       |        |      |      |      |      |

```

Q      B      FLOW 4 = BASE FLOW OF 750 CFS
Q      750.    61.      29.      128.
R      957.    963.
W      1.
SSEND

```

---

### 6.3.5 Bed Material Gradation

The initial gradation of material in the bed sediment control volume is described with PF (percent finer) and PFC (percent finer continuation) records. In Example Problem 3, this data has only been provided at Sections 1.0, 32.0, and 58.0 as noted in Field 2 of the PF records. The selection of which, and how many, cross sections at which to provide this data depends on study objectives, field data, etc. For intermediate cross sections HEC-6 will linearly interpolate the bed material gradation. Note that the points in the gradation tables need not coincide with the size classes selected for computation. See Appendix A for specific details of these data records.

### 6.3.6 Flow Data

The flow data input structure is similar to that shown in the previous examples. One of the differences, however, is the selection of A-, B- and C-level output for sediment computations on the Q records. Also, the hydrologic data are extremely important to the results of a movable bed simulation. Particular care must be taken when selecting the period of record or hypothetical event to be simulated and time step sizes to be used. Water temperature may also be important in some instances. See Gee (1984) and HEC (1992) for information regarding preparation of flow data.

### 6.3.7 Output of Sediment Model

Table 6-3b shows the output file for Example Problem 3. The geometric data output, similar to that produced by Example Problem 2, is followed by sediment data. At this point, no hydraulic or sediment transport computations have been performed. Rather, the input data have been read and manipulated in preparation for the computations which begin when the flow data are read. The sediment title records are echoed followed by the information on the I records. Next is the inflowing sediment load table from stream segment 1; the sediment loads are in scientific notation because of the wide range of possible values. Note that a very small value is used instead of zero because log-log interpolation is used within these data tables.

The table headed "REACH GEOMETRY FOR STREAM SEGMENT 1" depicts the status of the bed sediment control volume at the beginning of the simulation, as described by the input data. Note that the movable bed widths are not necessarily the same as given in the HD data. For example, at Section No. 1.0, the movable bed limits are specified at stations 10,081 and 10,250 which coincide with existing points in the GR data, therefore, these points are part of the movable bed. The movable bed width used for computations extends halfway to the next, fixed, GR points (at stations 10,077 and 10,275).

|                   |             |             |
|-------------------|-------------|-------------|
| Movable Bed Width | 10275 10250 | 10081 10077 |
|                   | 2           | 2           |
|                   | 183.5 ft    |             |



---

*Weighted VEL*   *XID*   *VEL at Downstream Section*

---

**Table 6-3b**  
**Example Problem 3 - Output**  
**Movable Bed**

```
*****
* SCOUR AND DEPOSITION IN RIVERS AND RESERVOIRS *
* Version: 4.1.00 - AUGUST 1993
* INPUT FILE: EXAMPLE3.DAT
* OUTPUT FILE: EXAMPLE3.OUT
* RUN DATE: 01 SEP 93 RUN TIME: 10:29:27
*****
* U. S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616-4687
* (916) 756-1104
*****
```

```

X   X   XXXXXXX   XXXXX   XXXXX
X   X   X         X   X     X   X
X   X   X         X         X
XXXXXX XXXX   X         XXXXX XXXXXX
X   X   X         X         X   X
X   X   X         X   X     X   X
X   X   XXXXXXX   XXXXX   XXXXX

```

```
*****
* MAXIMUM LIMITS FOR THIS VERSION ARE:
* 10 Stream Segments (Main Stem + Tributaries)
* 150 Cross Sections
* 100 Elevation/Station Points per Cross Section
* 20 Grain Sizes
* 10 Control Points
*****
```

```
T1 EXAMPLE PROBLEM NO 3. MOVABLE BED
T2 3 LOCAL INFLOWS
T3 SOUTH FORK, ZUMBRO RIVER ** Example Problem 3 **
```

```
N values... Left Channel Right Contraction Expansion
             0.1000 0.0400 0.1000 1.1000 0.7000
```

```
SECTION NO. 1.000
...DEPTH of the Bed Sediment Control Volume = 10.00 ft.
```

```
N-Values vs. Elevation Table
Channel Left Overbank Right Overbank
0.0450 966. 0.0800 966. 0.1000 966.
0.0640 989. 0.1300 989. 0.1100 982.
0.0000 0. 0.0000 0. 0.1200 989.
```

```
SECTION NO. 15.000
...Left Encroachment defined at station 10700.000 at elevation 961.000
...Right Encroachment defined at station 11000.000 at elevation 970.000
...DEPTH of the Bed Sediment Control Volume = 10.00 ft.
```

```
LOCAL INFLOW POINT 1 occurs upstream from Section No. 15.000
```

```
N values... Left Channel Right Contraction Expansion
             0.1000 0.0500 0.1000 1.1000 0.7000
```

```
SECTION NO. 32.000
...DEPTH of the Bed Sediment Control Volume = 10.00 ft.
```

```
SECTION NO. 32.100
...Ineffective Flow Area - Method 1 - Left Overbank Right Overbank
Natural Levees at Station 10057.000 10271.000
Ineffective Elevation 978.500 978.500
...DEPTH of the Bed Sediment Control Volume = 10.00 ft.
```

```
SECTION NO. 33.000
...Internal Boundary Condition
Water Surface Elevation will be read from R-RECORD, Field 2
Head Loss = 0.000
...Limit CONVEYANCE to 250.000 ft. centered about midpoint of channel.
...DEPTH of the Bed Sediment Control Volume = 0.00 ft.
```

```
SECTION NO. 33.300
...Adjust Section WIDTH to 95.00% of original.
...Adjust Section ELEVATIONS by 1.490 ft.
...Limit CONVEYANCE to 250.000 ft. centered about midpoint of channel.
...DEPTH of the Bed Sediment Control Volume = 0.00 ft.
```

```
SECTION NO. 33.900
...Adjust Section WIDTH to 95.00% of original.
...Adjust Section ELEVATIONS by 1.650 ft.
...Ineffective Flow Area - Method 1 - Left Overbank Right Overbank
Natural Levees at Station 1757.500 2042.500
Ineffective Elevation 986.060 986.150
...DEPTH of the Bed Sediment Control Volume = 0.00 ft.
```

```
SECTION NO. 35.000
...Internal Boundary Condition
Water Surface Elevation = 974.000
Head Loss = 0.500
```



...Ineffective Flow Area - Method 1 - Left Overbank Right Overbank  
 Natural Levees at Station 9894.000 10245.000  
 Ineffective Elevation 984.700 984.000

...DEPTH of the Bed Sediment Control Volume = 0.00 ft.

N values... Left Channel Right Contraction Expansion  
 0.0600 0.0450 0.0600 1.1000 0.7000

SECTION NO. 42.000

...DEPTH of the Bed Sediment Control Volume = 0.00 ft.

LOCAL INFLOW POINT 2 occurs upstream from Section No. 42.000

SECTION NO. 44.000

...Limit CONVEYANCE between stations 9850.000 and 10200.000  
 ...DEPTH of the Bed Sediment Control Volume = 1.00 ft.

SECTION NO. 53.000

...DEPTH of the Bed Sediment Control Volume = 10.00 ft.

LOCAL INFLOW POINT 3 occurs upstream from Section No. 53.000

SECTION NO. 55.000

...DEPTH of the Bed Sediment Control Volume = 10.00 ft.

SECTION NO. 58.000

...DEPTH of the Bed Sediment Control Volume = 3.40 ft.

NO. OF CROSS SECTIONS IN STREAM SEGMENT= 13

NO. OF INPUT DATA MESSAGES = 0

TOTAL NO. OF CROSS SECTIONS IN THE NETWORK = 13

TOTAL NO. OF STREAM SEGMENTS IN THE NETWORK= 1

END OF GEOMETRIC DATA

T4 South Fork, Zumbro River - Stream Segment 1 \*\* Example Problem 3 \*\*  
 T5 LOAD CURVE FROM GAGE DATA.  
 T6 BED GRADATIONS FROM FIELD SAMPLES.  
 T7 Use Full Range of Sands and Gravels  
 T8 SEDIMENT TRANSPORT BY Yang's STREAM POWER [ref ASCE JOURNAL (YANG 1971)]

EXAMPLE PROBLEM NO 3. MOVABLE BED  
 3 LOCAL INFLOWS  
 SOUTH FORK, ZUMBRO RIVER \*\* Example Problem 3 \*\*

-----  
 SEDIMENT PROPERTIES AND PARAMETERS

| I1 | SPI | IBG | MNQ | SPGF  | ACGR   | NFALL | IBSHER |
|----|-----|-----|-----|-------|--------|-------|--------|
|    | 5.  | 0   | 1   | 1.000 | 32.174 | 2     | 1      |

SANDS - BOULDERS ARE PRESENT

| I4 | MTC | IASA | LASA | SPGS  | GSF   | BSAE  | PSI    | UWDLB  |
|----|-----|------|------|-------|-------|-------|--------|--------|
|    | 4   | 1    | 10   | 2.650 | 0.667 | 0.500 | 30.000 | 93.000 |

USING TRANSPORT CAPACITY RELATIONSHIP # 4, YANG

GRAIN SIZES UTILIZED (mean diameter - mm)

|                    |       |                    |        |
|--------------------|-------|--------------------|--------|
| VERY FINE SAND.... | 0.088 | VERY FINE GRAVEL.. | 2.828  |
| FINE SAND.....     | 0.177 | FINE GRAVEL.....   | 5.657  |
| MEDIUM SAND.....   | 0.354 | MEDIUM GRAVEL....  | 11.314 |
| COARSE SAND.....   | 0.707 | COARSE GRAVEL....  | 22.627 |
| VERY COARSE SAND.. | 1.414 | VERY COARSE GRAVEL | 45.255 |

COEFFICIENTS FOR COMPUTATION SCHEME WERE SPECIFIED

| I5 | DBI   | DBN   | XID   | XIN   | XIU   | UBI   | UBN   | JSL |
|----|-------|-------|-------|-------|-------|-------|-------|-----|
|    | 0.500 | 0.500 | 0.250 | 0.500 | 0.250 | 0.000 | 1.000 | 1   |

-----  
 SEDIMENT LOAD TABLE FOR STREAM SEGMENT # 1  
 LOAD BY GRAIN SIZE CLASS (tons/day)

| LQ    |     | 1.00000      | 50.0000      | 1000.00      | 5800.00      | 90000.0      |
|-------|-----|--------------|--------------|--------------|--------------|--------------|
| LF    | VFS | 0.130900E-02 | 0.178500     | 159.360      | 2299.50      | 232800.      |
| LF    | FS  | 0.360800E-02 | 0.492000     | 105.920      | 1377.00      | 112000.      |
| LF    | MS  | 0.608300E-02 | 0.829500     | 49.9200      | 693.000      | 44000.0      |
| LF    | CS  | 0.100000E-19 | 0.100000E-19 | 3.52000      | 72.0000      | 8000.00      |
| LF    | VCS | 0.100000E-19 | 0.100000E-19 | 1.28000      | 36.0000      | 2000.00      |
| LF    | VFG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 18.0000      | 800.000      |
| LF    | FG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 4.50000      | 400.000      |
| LF    | ME  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 |
| LF    | CG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 |
| LF    | VCG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 |
| TOTAL |     | 0.110000E-01 | 1.50000      | 320.000      | 4500.00      | 400000.      |

REACH GEOMETRY FOR STREAM SEGMENT 1

| CROSS SECTION NO. | REACH LENGTH (ft) | MOVABLE BED WIDTH | INITIAL LEFT SIDE (ft) | BED THALWEG (ft) | ELEVATIONS RIGHT SIDE (ft) | ACCUMULATED FROM DOWNSTREAM (ft) | CHANNEL DISTANCE (miles) |
|-------------------|-------------------|-------------------|------------------------|------------------|----------------------------|----------------------------------|--------------------------|
| 1.000             | 0.000             | 183.500           | 959.300                | 944.700          | 958.900                    | 0.000                            | 0.000                    |
| 15.000            | 3280.000          | 242.000           | 961.000                | 953.700          | 962.000                    | 3280.000                         | 0.621                    |
| 32.000            | 4240.000          | 219.500           | 968.600                | 956.500          | 978.500                    | 7520.000                         | 1.424                    |
| 32.100            | 3320.000          | 219.500           | 968.600                | 956.500          | 978.500                    | 10840.000                        | 2.053                    |
| 33.000            | 0.000             | 299.000           | 979.190                | 961.000          | 976.000                    | 10840.000                        | 2.053                    |
| 33.300            | 1750.000          | 284.050           | 980.680                | 962.490          | 977.490                    | 12590.000                        | 2.384                    |
| 33.900            | 1050.000          | 284.050           | 980.840                | 962.650          | 977.650                    | 13640.000                        | 2.583                    |
| 35.000            | 0.000             | 275.950           | 963.300                | 963.300          | 983.700                    | 13640.000                        | 2.583                    |
| 42.000            | 5210.000          | 154.500           | 969.800                | 969.800          | 969.800                    | 18850.000                        | 3.570                    |
| 44.000            | 3500.000          | 337.500           | 970.900                | 967.100          | 976.900                    | 22350.000                        | 4.233                    |
| 53.000            | 2942.000          | 195.000           | 982.800                | 972.200          | 988.700                    | 25292.000                        | 4.790                    |
| 55.000            | 2770.000          | 204.000           | 987.200                | 972.900          | 983.800                    | 28062.000                        | 5.315                    |
| 58.000            | 1462.000          | 176.500           | 996.300                | 975.400          | 990.400                    | 29524.000                        | 5.592                    |

BED MATERIAL GRADATION

| SECCO  | SAE   | DMAX (ft) | DXPI (ft) | XPI   | TOTAL BED | BED MATERIAL FRACTIONS per grain size |       |         |       |        |       |        |       |         |       |        |       |        |       |        |       |         |       |        |       |
|--------|-------|-----------|-----------|-------|-----------|---------------------------------------|-------|---------|-------|--------|-------|--------|-------|---------|-------|--------|-------|--------|-------|--------|-------|---------|-------|--------|-------|
| 1.000  | 1.000 | 0.105     | 0.105     | 1.000 | 1.000     | VF SAND                               | 0.010 | VC SAND | 0.120 | M GRVL | 0.015 | F SAND | 0.070 | VF GRVL | 0.060 | C GRVL | 0.035 | M SAND | 0.290 | F GRVL | 0.040 | VC GRVL | 0.000 | C SAND | 0.360 |
| 15.000 | 1.000 | 0.151     | 0.151     | 1.000 | 1.000     | VF SAND                               | 0.010 | VC SAND | 0.113 | M GRVL | 0.011 | F SAND | 0.070 | VF GRVL | 0.045 | C GRVL | 0.022 | M SAND | 0.327 | F GRVL | 0.033 | VC GRVL | 0.002 | C SAND | 0.367 |
| 32.000 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.010 | VC SAND | 0.105 | M GRVL | 0.005 | F SAND | 0.070 | VF GRVL | 0.025 | C GRVL | 0.005 | M SAND | 0.375 | F GRVL | 0.025 | VC GRVL | 0.005 | C SAND | 0.375 |
| 32.100 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.008 | VC SAND | 0.124 | M GRVL | 0.004 | F SAND | 0.062 | VF GRVL | 0.038 | C GRVL | 0.009 | M SAND | 0.321 | F GRVL | 0.027 | VC GRVL | 0.009 | C SAND | 0.397 |
| 33.000 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.008 | VC SAND | 0.124 | M GRVL | 0.004 | F SAND | 0.062 | VF GRVL | 0.038 | C GRVL | 0.009 | M SAND | 0.321 | F GRVL | 0.027 | VC GRVL | 0.009 | C SAND | 0.397 |
| 33.300 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.008 | VC SAND | 0.134 | M GRVL | 0.004 | F SAND | 0.058 | VF GRVL | 0.045 | C GRVL | 0.011 | M SAND | 0.293 | F GRVL | 0.028 | VC GRVL | 0.011 | C SAND | 0.408 |
| 33.900 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.007 | VC SAND | 0.140 | M GRVL | 0.004 | F SAND | 0.056 | VF GRVL | 0.049 | C GRVL | 0.012 | M SAND | 0.276 | F GRVL | 0.029 | VC GRVL | 0.012 | C SAND | 0.415 |
| 35.000 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.007 | VC SAND | 0.140 | M GRVL | 0.004 | F SAND | 0.056 | VF GRVL | 0.049 | C GRVL | 0.012 | M SAND | 0.276 | F GRVL | 0.029 | VC GRVL | 0.012 | C SAND | 0.415 |
| 42.000 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.005 | VC SAND | 0.169 | M GRVL | 0.002 | F SAND | 0.044 | VF GRVL | 0.069 | C GRVL | 0.018 | M SAND | 0.192 | F GRVL | 0.033 | VC GRVL | 0.018 | C SAND | 0.450 |
| 44.000 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.003 | VC SAND | 0.189 | M GRVL | 0.002 | F SAND | 0.036 | VF GRVL | 0.082 | C GRVL | 0.022 | M SAND | 0.136 | F GRVL | 0.035 | VC GRVL | 0.022 | C SAND | 0.473 |
| 53.000 | 1.000 | 0.210     | 0.210     | 1.000 | 1.000     | VF SAND                               | 0.002 | VC SAND | 0.206 | M GRVL | 0.001 | F SAND | 0.030 | VF GRVL | 0.094 | C GRVL | 0.025 | M SAND | 0.088 | F GRVL | 0.037 | VC GRVL | 0.025 | C SAND | 0.492 |

|        |       |       |       |       |       |               |               |               |
|--------|-------|-------|-------|-------|-------|---------------|---------------|---------------|
| 55.000 | 1.000 | 0.210 | 0.210 | 1.000 | 1.000 | VF SAND 0.001 | VC SAND 0.222 | M GRVL 0.000  |
|        |       |       |       |       |       | F SAND 0.023  | VF GRVL 0.104 | C GRVL 0.028  |
|        |       |       |       |       |       | M SAND 0.044  | F GRVL 0.039  | VC GRVL 0.028 |
|        |       |       |       |       |       | C SAND 0.510  |               |               |
| 58.000 | 1.000 | 0.210 | 0.210 | 1.000 | 1.000 | VF SAND 0.000 | VC SAND 0.230 | M GRVL 0.000  |
|        |       |       |       |       |       | F SAND 0.020  | VF GRVL 0.110 | C GRVL 0.030  |
|        |       |       |       |       |       | M SAND 0.020  | F GRVL 0.040  | VC GRVL 0.030 |
|        |       |       |       |       |       | C SAND 0.520  |               |               |

.. LOCAL INFLOW DATA ..

SEDIMENT LOAD TABLE FOR STREAM SEGMENT # 1  
 AT LOCAL INFLOW POINT # 1  
 LOAD BY GRAIN SIZE CLASS (tons/day)

| LQL     | 1.00000      | 100.000      | 1000.00      | 10000.0 |
|---------|--------------|--------------|--------------|---------|
| LFL VFS | 0.265600E-02 | 6.64000      | 7.50000      | 5940.00 |
| LFL FS  | 0.828000E-03 | 2.07000      | 122.500      | 5430.00 |
| LFL MS  | 0.344000E-03 | 0.860000     | 302.500      | 3210.00 |
| LFL CS  | 0.124000E-03 | 0.310000     | 26.0000      | 2940.00 |
| LFL VCS | 0.320000E-04 | 0.800000E-01 | 19.5000      | 3810.00 |
| LFL VFG | 0.120000E-04 | 0.300000E-01 | 10.0000      | 3480.00 |
| LFL FG  | 0.400000E-05 | 0.100000E-01 | 5.50000      | 2730.00 |
| LFL ME  | 0.100000E-19 | 0.100000E-19 | 5.50000      | 1590.00 |
| LFL CG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 660.000 |
| LFL VCG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 180.000 |
| TOTAL   | 0.400000E-02 | 10.0000      | 499.000      | 29970.0 |

SEDIMENT LOAD TABLE FOR STREAM SEGMENT # 1  
 AT LOCAL INFLOW POINT # 2  
 LOAD BY GRAIN SIZE CLASS (tons/day)

| LQL     | 1.00000      | 100.000      | 1000.00      | 10000.0 |
|---------|--------------|--------------|--------------|---------|
| LFL VFS | 0.265600E-02 | 6.64000      | 7.50000      | 5940.00 |
| LFL FS  | 0.828000E-03 | 2.07000      | 122.500      | 5430.00 |
| LFL MS  | 0.344000E-03 | 0.860000     | 302.500      | 3210.00 |
| LFL CS  | 0.124000E-03 | 0.310000     | 26.0000      | 2940.00 |
| LFL VCS | 0.320000E-04 | 0.800000E-01 | 19.5000      | 3810.00 |
| LFL VFG | 0.120000E-04 | 0.300000E-01 | 10.0000      | 3480.00 |
| LFL FG  | 0.400000E-05 | 0.100000E-01 | 5.50000      | 2730.00 |
| LFL ME  | 0.100000E-19 | 0.100000E-19 | 5.50000      | 1590.00 |
| LFL CG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 660.000 |
| LFL VCG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 180.000 |
| TOTAL   | 0.400000E-02 | 10.0000      | 499.000      | 29970.0 |

SEDIMENT LOAD TABLE FOR STREAM SEGMENT # 1  
 AT LOCAL INFLOW POINT # 3  
 LOAD BY GRAIN SIZE CLASS (tons/day)

| LQL     | 1.00000      | 100.000      | 500.000      | 1000.00      | 30000.0      |
|---------|--------------|--------------|--------------|--------------|--------------|
| LFL VFS | 0.402000E-03 | 6.03000      | 39.0000      | 93.6000      | 3082.50      |
| LFL FS  | 0.684000E-03 | 10.2600      | 86.0000      | 210.000      | 4905.00      |
| LFL MS  | 0.902000E-03 | 13.5300      | 227.000      | 721.200      | 10710.0      |
| LFL CS  | 0.200000E-05 | 0.300000E-01 | 98.5000      | 170.400      | 3555.00      |
| LFL VCS | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 3.60000      | 180.000      |
| LFL VFG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 45.0000      |
| LFL FG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 22.5000      |
| LFL ME  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 |
| LFL CG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 |
| LFL VCG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 |
| TOTAL   | 0.199000E-02 | 29.8500      | 450.500      | 1198.80      | 22500.0      |

BED SEDIMENT CONTROL VOLUMES

STREAM SEGMENT # 1: EXAMPLE PROBLEM NO 3. MOVABLE BED

| SECTION NUMBER | LENGTH (ft) | WIDTH (ft) | DEPTH (ft) | VOLUME (cu. ft) | VOLUME (cu. yd) |
|----------------|-------------|------------|------------|-----------------|-----------------|
| 1.000          | 1640.000    | 203.000    | 10.000     | 0.332920E+07    | 123304.         |
| 15.000         | 3760.000    | 229.266    | 10.000     | 0.862040E+07    | 319274.         |
| 32.000         | 3780.000    | 223.706    | 10.000     | 0.845610E+07    | 313189.         |
| 32.100         | 1660.000    | 219.500    | 10.000     | 0.364370E+07    | 134952.         |
| 33.000         | 875.000     | 294.017    | 0.000      | 0.000000        | 0.000000        |
| 33.300         | 1400.000    | 287.165    | 0.000      | 0.000000        | 0.000000        |
| 33.900         | 525.000     | 284.050    | 0.000      | 0.000000        | 0.000000        |
| 35.000         | 2605.000    | 235.467    | 0.000      | 0.000000        | 0.000000        |
| 42.000         | 4355.000    | 203.228    | 0.000      | 0.000000        | 0.000000        |
| 44.000         | 3221.000    | 282.665    | 1.000      | 910465.         | 33720.9         |
| 53.000         | 2856.000    | 220.920    | 10.000     | 0.630947E+07    | 233684.         |
| 55.000         | 2116.000    | 198.870    | 10.000     | 0.420808E+07    | 155855.         |
| 58.000         | 731.000     | 185.667    | 3.400      | 461456.         | 17091.0         |

NO. OF INPUT DATA MESSAGES= 0  
 END OF SEDIMENT DATA

SHYD  
BEGIN COMPUTATIONS.

=====

TIME STEP # 1  
Q A FLOW 1 = BASE FLOW OF 750 CFS

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
EXAMPLE PROBLEM NO 3. MOVABLE BED  
ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```

*****
TIME      ENTRY *      SAND
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
2.00     58.000 *      0.09   0.00    1.00 *
          53.000 *      0.04   0.00    1.00 *
          42.000 *      0.00   0.00    1.00 *
TOTAL=   35.000 *      0.14   0.00    1.00 *
*****
TIME      ENTRY *      SAND
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
2.00     35.000 *      0.00   0.00    0.49 *
TOTAL=   33.000 *      0.00   0.00    0.49 *
*****
TIME      ENTRY *      SAND
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
2.00     33.000 *      0.00   0.00    3.36 *
          15.000 *      0.00   0.00    3.36 *
TOTAL=   1.000 *      0.00   0.02   -3.36 *
*****
    
```

=====

TIME STEP # 2  
Q B FLOW 2 = 50 DAYS AT BANK FULL DISCHARGE

EXAMPLE PROBLEM NO 3. MOVABLE BED  
ACCUMULATED TIME (yrs).... 0.142  
FLOW DURATION (days)..... 50.000

UPSTREAM BOUNDARY CONDITIONS

| Stream Segment # 1<br>Section No.                 | DISCHARGE<br>(cfs) | SEDIMENT LOAD<br>(tons/day) | TEMPERATURE<br>(deg F) |
|---|--------------------|-----------------------------|------------------------|
| INFLOW  | 1400.00            | 529.98                      | 62.04                  |
| Upstream of SECTION NO.<br>LOCAL INFLOW POINT # 3 |                    |                             |                        |
| DISCHARGE   | 53.000 is...       | SEDIMENT LOAD               | TEMPERATURE            |
| (cfs)   |                    | (tons/day)                  | (deg F)                |
| MAIN STEM INFLOW                                  | 1400.00            | 529.98                      | 62.04                  |
| LOCAL INFLOW                                      | 650.00             | 647.71                      | 67.00                  |
| TOTAL   | 2050.00            | 1177.69                     | 63.61                  |
| Upstream of SECTION NO.<br>LOCAL INFLOW POINT # 2 |                    |                             |                        |
| DISCHARGE   | 42.000 is...       | SEDIMENT LOAD               | TEMPERATURE            |
| (cfs)   |                    | (tons/day)                  | (deg F)                |
| MAIN STEM INFLOW                                  | 2050.00            | 1177.69                     | 63.61                  |
| LOCAL INFLOW                                      | 150.00             | 14.45                       | 70.00                  |
| TOTAL   | 2200.00            | 1192.13                     | 64.05                  |
| Upstream of SECTION NO.<br>LOCAL INFLOW POINT # 1 |                    |                             |                        |
| DISCHARGE   | 15.000 is...       | SEDIMENT LOAD               | TEMPERATURE            |
| (cfs)   |                    | (tons/day)                  | (deg F)                |
| MAIN STEM INFLOW                                  | 2200.00            | 1192.13                     | 64.05                  |
| LOCAL INFLOW                                      | 300.00             | 40.00                       | 72.00                  |
| TOTAL   | 2500.00            | 1232.13                     | 65.00                  |

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
EXAMPLE PROBLEM NO 3. MOVABLE BED  
ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```

*****
TIME      ENTRY *      SAND
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
52.00    58.000 *      13.17   5.51    0.81 *
          53.000 *      16.03   1.47    0.73 *
          42.000 *      0.36   0.00    0.97 *
TOTAL=   35.000 *      29.56   5.51    0.97 *
*****
TIME      ENTRY *      SAND
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
52.00    35.000 *      5.51   1.47    0.73 *
TOTAL=   33.000 *      5.51   1.47    0.73 *
*****
TIME      ENTRY *      SAND
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
52.00    33.000 *      1.47   0.00    0.97 *
          15.000 *      0.99   0.00    0.97 *
TOTAL=   1.000 *      2.46   0.07    0.97 *
*****
    
```

TABLE SB-1: SEDIMENT LOAD PASSING THE BOUNDARIES OF STREAM SEGMENT # 1

| SEDIMENT INFLOW at the Upstream Boundary:     |                 |                    |                 |
|---|-----------------|--------------------|-----------------|
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |
| VERY FINE SAND...                             | 265.63          | VERY FINE GRAVEL.. | 0.00            |
| FINE SAND.....                                | 173.06          | FINE GRAVEL.....   | 0.00            |
| MEDIUM SAND.....                              | 82.59           | MEDIUM GRAVEL..... | 0.00            |
| COARSE SAND.....                              | 6.27            | COARSE GRAVEL..... | 0.00            |
| VERY COARSE SAND..                            | 2.42            | VERY COARSE GRAVEL | 0.00            |
|   |                 |                    | TOTAL = 529.98  |
| SEDIMENT OUTFLOW from the Downstream Boundary |                 |                    |                 |
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |
| VERY FINE SAND...                             | 0.24            | VERY FINE GRAVEL.. | 0.00            |
| FINE SAND.....                                | 0.27            | FINE GRAVEL.....   | 0.00            |
| MEDIUM SAND.....                              | 0.72            | MEDIUM GRAVEL..... | 0.00            |
| COARSE SAND.....                              | 0.59            | COARSE GRAVEL..... | 0.00            |
| VERY COARSE SAND..                            | 0.13            | VERY COARSE GRAVEL | 0.00            |
|   |                 |                    | TOTAL = 1.94    |

TABLE SB-2: STATUS OF THE BED PROFILE AT TIME = 52.000 DAYS

| SECTION NUMBER | BED CHANGE (ft) | WS ELEV (ft) | THALWEG (ft) | Q (cfs) | TRANSPORT RATE (tons/day) SAND |
|----------------|-----------------|--------------|--------------|---------|--------------------------------|
| 58.000         | -0.60           | 981.86       | 974.80       | 1400.   | 557.                           |
| 55.000         | 0.10            | 980.67       | 973.00       | 1400.   | 525.                           |
| 53.000         | 0.40            | 977.12       | 972.60       | 2050.   | 1044.                          |
| 44.000         | 0.08            | 975.90       | 967.18       | 2050.   | 1014.                          |
| 42.000         | 0.92            | 975.15       | 970.72       | 2200.   | 300.                           |
| 35.000         | 0.17            | 974.00       | 963.47       | 2200.   | 223.                           |
| 33.900         | 0.57            | 970.36       | 963.22       | 2200.   | 160.                           |
| 33.300         | 0.12            | 970.19       | 962.61       | 2200.   | 124.                           |
| 33.000         | 0.33            | 970.00       | 961.33       | 2200.   | 59.                            |
| 32.100         | -0.19           | 967.63       | 956.31       | 2200.   | 105.                           |
| 32.000         | -0.13           | 966.55       | 956.37       | 2200.   | 157.                           |
| 15.000         | -0.19           | 965.13       | 953.51       | 2500.   | 232.                           |
| 1.000          | 1.03            | 965.00       | 945.73       | 2500.   | 2.                             |

SPRT  
 ...Selective Printout Option  
 - Print at the following cross sections  
 CP 1  
 PS 15.0 32.0 32.1  
 END

=====

TIME STEP # 3  
 Q AC FLOW 3 = NEAR BANK FULL DISCHARGE

EXAMPLE PROBLEM NO 3. MOVABLE BED  
 ACCUMULATED TIME (yrs)..... 0.142

--- Downstream Boundary Condition Data for STREAM SEGMENT NO. 1 at Control Point # 1 ---

|                      | DISCHARGE (cfs) | TEMPERATURE (deg F) | WATER SURFACE (ft) | AVG VEL (by subsection) |       |         |         |                         |         |       |
|----------------------|-----------------|---------------------|--------------------|-------------------------|-------|---------|---------|-------------------------|---------|-------|
|                      |                 |                     |                    | 1                       | 2     | 3       |         |                         |         |       |
|                      | 1250.000        | 65.00               | 960.000            |                         |       |         |         |                         |         |       |
| **** DISCHARGE (CFS) | 1250.000        | 960.477             | 960.622            | 0.144                   | 1.000 | 144.463 | 957.639 | 0.000                   | 3.048   | 0.000 |
| SECTION NO.          | 15.000          |                     |                    |                         |       |         |         |                         |         |       |
| ****                 |                 |                     |                    |                         |       |         |         | 0.000                   | 100.000 | 0.000 |
|                      |                 |                     |                    |                         |       |         |         | FLOW DISTRIBUTION (%) = |         |       |

--- LOCAL INFLOW POINT # 1 is upstream of Section No. 15.000 ---

|               | DISCHARGE (cfs) | TEMPERATURE (deg F) | AVG VEL (by subsection) |       |       |         |         |                         |       |       |
|---------------|-----------------|---------------------|-------------------------|-------|-------|---------|---------|-------------------------|-------|-------|
|               |                 |                     | 1                       | 2     | 3     |         |         |                         |       |       |
| Local Inflow: | 150.000         | 72.00               |                         |       |       |         |         |                         |       |       |
| Total:        | 1100.000        | 64.05               |                         |       |       |         |         |                         |       |       |
| SECTION NO.   | 32.000          |                     |                         |       |       |         |         |                         |       |       |
| ****          | 1100.000        | 963.899             | 963.941                 | 0.042 | 1.000 | 132.795 | 958.838 | 0.000                   | 1.637 | 0.000 |
|               |                 |                     |                         |       |       |         |         | FLOW DISTRIBUTION (%) = |       |       |
| SECTION NO.   | 32.100          |                     |                         |       |       |         |         |                         |       |       |
| ****          | 1100.000        | 964.813             | 964.842                 | 0.029 | 1.000 | 138.333 | 959.013 | 0.000                   | 1.371 | 0.000 |
|               |                 |                     |                         |       |       |         |         | FLOW DISTRIBUTION (%) = |       |       |

EXAMPLE PROBLEM NO 3. MOVABLE BED  
 ACCUMULATED TIME (yrs).... 0.145  
 FLOW DURATION (days)..... 1.000

UPSTREAM BOUNDARY CONDITIONS

| Stream Segment #   | DISCHARGE (cfs) | SEDIMENT LOAD (tons/day) | TEMPERATURE (deg F) |
|--------------------|-----------------|--------------------------|---------------------|
| Section No. 58.000 |                 |                          |                     |
| INFLOW             | 682.00          | 149.81                   | 61.89               |

| SEDIMENT INFLOW at SECTION NO. 58.000 |                 |                      |                 |
|---------------------------------------|-----------------|----------------------|-----------------|
| GRAIN SIZE                            | LOAD (tons/day) | GRAIN SIZE           | LOAD (tons/day) |
| VERY FINE SAND. . . .                 | 66.90           | VERY FINE GRAVEL. .  | 0.00            |
| FINE SAND. . . . .                    | 53.32           | FINE GRAVEL. . . . . | 0.00            |
| MEDIUM SAND. . . . .                  | 29.58           | MEDIUM GRAVEL. . . . | 0.00            |
| COARSE SAND. . . . .                  | 0.01            | COARSE GRAVEL. . . . | 0.00            |
| VERY COARSE SAND. .                   | 0.00            | VERY COARSE GRAVEL   | 0.00            |
|                                       |                 | TOTAL =              | 149.81          |

| FALL VELOCITIES - Method 2 |          |               |           |          |
|----------------------------|----------|---------------|-----------|----------|
|                            | DIAMETER | VELOCITY      | REY. NO.  | CD       |
| VF SAND                    | 0.000290 | 0.1860300E-01 | 0.4558130 | 59.31192 |
| F SAND                     | 0.000580 | 0.5765145E-01 | 2.825166  | 12.35143 |
| M SAND                     | 0.001160 | 0.1327884     | 13.01437  | 4.656360 |
| C SAND                     | 0.002320 | 0.2803304     | 54.94943  | 2.089569 |
| VC SAND                    | 0.004640 | 0.4807405     | 188.4667  | 1.421041 |
| VF GRVL                    | 0.009280 | 0.7191215     | 563.8404  | 1.270145 |
| F GRVL                     | 0.018559 | 1.039704      | 1630.395  | 1.215254 |
| M GRVL                     | 0.037118 | 1.472894      | 4619.401  | 1.211086 |
| C GRVL                     | 0.074237 | 2.082985      | 13065.61  | 1.211086 |
| VC GRVL                    | 0.148474 | 2.945788      | 36955.21  | 1.211086 |

\*\*\*\*\*  
TRACE OUTPUT FOR SECTION NO. 32.100  
\*\*\*\*\*

| HYDRAULIC PARAMETERS: |          |       |         |         |         |         |            |
|-----------------------|----------|-------|---------|---------|---------|---------|------------|
| VEL                   | SLO      | efd   | efw     | N-VALUE | TAU     | USTARM  | FROUDE NO. |
| 1.371                 | 0.000271 | 6.763 | 118.634 | 0.0500  | 0.11467 | 0.24306 | 0.093      |

| BED SEDIMENT CONTROL VOLUME COMPUTATIONS: |           |           |           |
|---|-----------|-----------|-----------|
| NEW SURFACE AREA (SQ FT):                 | TOTAL     | K-PORTION | S-PORTION |
|   | 214970.00 | 214970.00 | 0.00      |

| GRADATION OF ACTIVE PLUS INACTIVE DEPOSITS |              |               |         |              |               |  |  |
|--|--------------|---------------|---------|--------------|---------------|--|--|
| BED MATERIAL PER GRAIN SIZE:               | BED FRACTION | PERCENT FINER |         | BED FRACTION | PERCENT FINER |  |  |
| VF SAND                                    | 0.012074     | 1.207441      | VF GRVL | 0.038537     | 94.998190     |  |  |
| F SAND                                     | 0.062093     | 7.416711      | F GRVL  | 0.027800     | 97.778156     |  |  |
| M SAND                                     | 0.319568     | 39.373478     | M GRVL  | 0.004329     | 98.211069     |  |  |
| C SAND                                     | 0.394570     | 78.830455     | C GRVL  | 0.008945     | 99.105534     |  |  |
| VC SAND                                    | 0.123140     | 91.144443     | VC GRVL | 0.008945     | 99.999998     |  |  |

SAND  
\*\* ARMOR LAYER \*\*  
STABILITY COEFFICIENT= 0.81992  
MN. GRAIN DIAM = 0.001943  
BED SURFACE EXPOSED = 0.28365

|       | INACTIVE LAYER |       | ACTIVE LAYER |       |
|-------|----------------|-------|--------------|-------|
|       | %              | DEPTH | %            | DEPTH |
| CLAY  | 0.0000         | 0.00  | 0.0000       | 0.00  |
| SILT  | 0.0000         | 0.00  | 0.0000       | 0.00  |
| SAND  | 1.0000         | 9.76  | 1.0000       | 0.05  |
| TOTAL | 1.0000         | 9.76  | 1.0000       | 0.05  |

| AVG. UNIT WEIGHT | AVG. UNIT WEIGHT |
|------------------|------------------|
| 0.046500         | 0.046500         |

COMPOSITE UNIT WT OF ACTIVE LAYER (t/cf)= 0.046500  
COMPOSITE UNIT WT OF INACTIVE LAYER (t/cf)= 0.046500  
DEPTH OF SURFACE LAYER (ft) DSL= 0.1  
WEIGHT IN SURFACE LAYER (tons) WTSL= 833.0  
DEPTH OF NEW ACTIVE LAYER (ft) DSE= 0.0008  
WEIGHT IN NEW ACTIVE LAYER(tons) WTMAL= 7.6  
WEIGHT IN OLD ACTIVE LAYER(tons) WAL= 497.7  
USEABLE WEIGHT, OLD INACTIVE LAYER WIL= 97534.4  
SURFACE AREA OF DEPOSIT (sq ft) SABK= 0.21497000E+06

| ** INACTIVE LAYER **   |         |              |               |         |              |               |  |
|------------------------|---------|--------------|---------------|---------|--------------|---------------|--|
| BED MATERIAL PER GRAIN | SIZE:   | BED FRACTION | PERCENT FINER |         | BED FRACTION | PERCENT FINER |  |
|                        | VF SAND | 0.008485     | 0.848488      | VF GRVL | 0.038120     | 95.056453     |  |
|                        | F SAND  | 0.062410     | 7.089446      | F GRVL  | 0.027476     | 97.804037     |  |
|                        | M SAND  | 0.321199     | 39.209296     | M GRVL  | 0.004279     | 98.231907     |  |
|                        | C SAND  | 0.396583     | 78.867631     | C GRVL  | 0.008840     | 99.115953     |  |
|                        | VC SAND | 0.123768     | 91.244461     | VC GRVL | 0.008840     | 99.999998     |  |

| ** ACTIVE LAYER **     |         |              |               |         |              |               |  |
|------------------------|---------|--------------|---------------|---------|--------------|---------------|--|
| BED MATERIAL PER GRAIN | SIZE:   | BED FRACTION | PERCENT FINER |         | BED FRACTION | PERCENT FINER |  |
|                        | VF SAND | 0.715456     | 71.545615     | VF GRVL | 0.120357     | 83.581306     |  |
|                        | F SAND  | 0.000000     | 71.545615     | F GRVL  | 0.091254     | 92.706690     |  |
|                        | M SAND  | 0.000000     | 71.545615     | M GRVL  | 0.014211     | 94.127749     |  |
|                        | C SAND  | 0.000000     | 71.545615     | C GRVL  | 0.029361     | 97.063875     |  |
|                        | VC SAND | 0.000000     | 71.545615     | VC GRVL | 0.029361     | 100.000000    |  |

C FINES, COEF(CFFML), MK POTENTIAL= 0.000000E+00 0.100000E+01 0.237600E+07  
POTENTIAL TRANSPORT (tons/day): VF SAND 0.560062E+03 VF GRVL 0.100000E-06  
F SAND 0.199470E+03 F GRVL 0.100000E-06  
M SAND 0.125719E+03 M GRVL 0.100000E-06  
C SAND 0.947155E+02 C GRVL 0.100000E-06  
VC SAND 0.765651E+02 VC GRVL 0.100000E-06

| SEDIMENT OUTFLOW FROM SECTION NO. 32.100 |                 | GRAIN SIZE LOAD (tons/day)  |                 |
|--|-----------------|-----------------------------|-----------------|
| GRAIN SIZE                               | LOAD (tons/day) | GRAIN SIZE                  | LOAD (tons/day) |
| VERY FINE SAND. . . . .                  | 148.98          | VERY FINE GRAVEL. . . . .   | 0.00            |
| FINE SAND. . . . .                       | 9.07            | FINE GRAVEL. . . . .        | 0.00            |
| MEDIUM SAND. . . . .                     | 23.59           | MEDIUM GRAVEL. . . . .      | 0.00            |
| COARSE SAND. . . . .                     | 21.05           | COARSE GRAVEL. . . . .      | 0.00            |
| VERY COARSE SAND. . . . .                | 5.30            | VERY COARSE GRAVEL. . . . . | 0.00            |

\*\*\*\*\*

TRACE OUTPUT FOR SECTION NO. 32.000

HYDRAULIC PARAMETERS:

| VEL   | SLO      | EFD   | EFW     | N-VALUE | TAU     | USTARM  | FROUDE NO. |
|-------|----------|-------|---------|---------|---------|---------|------------|
| 1.923 | 0.000527 | 5.733 | 110.118 | 0.0500  | 0.18875 | 0.31184 | 0.142      |

BED SEDIMENT CONTROL VOLUME COMPUTATIONS:

| NEW SURFACE AREA (SQ FT): | TOTAL     | K-PORTION | S-PORTION |
|---------------------------|-----------|-----------|-----------|
|                           | 495163.69 | 495163.69 | 0.00      |

GRADATION OF ACTIVE PLUS INACTIVE DEPOSITS

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0.011063     | 1.106303      | VF GRVL      | 0.025317      |
| F SAND                       | 0.070203     | 8.126581      | F GRVL       | 0.025337      |
| M SAND                       | 0.374483     | 45.574892     | M GRVL       | 0.005068      |
| C SAND                       | 0.373745     | 82.949358     | C GRVL       | 0.005068      |
| VC SAND                      | 0.104649     | 93.414209     | VC GRVL      | 0.005068      |

SAND

\*\* ARMOR LAYER \*\*  
 STABILITY COEFFICIENT= 0.76487  
 MN. GRAIN DIAM = 0.003170  
 BED SURFACE EXPOSED = 1.00000

|       | INACTIVE LAYER | ACTIVE LAYER |
|-------|----------------|--------------|
|       | % DEPTH        | % DEPTH      |
| CLAY  | 0.0000 0.00    | 0.0000 0.00  |
| SILT  | 0.0000 0.00    | 0.0000 0.00  |
| SAND  | 1.0000 9.84    | 1.0000 0.03  |
| TOTAL | 1.0000 9.84    | 1.0000 0.03  |

| AVG. UNIT WEIGHT | AVG. UNIT WEIGHT |
|------------------|------------------|
| 0.046500         | 0.046500         |

COMPOSITE UNIT WT OF ACTIVE LAYER (t/cf)= 0.046500  
 COMPOSITE UNIT WT OF INACTIVE LAYER (t/cf)= 0.046500  
 DEPTH OF SURFACE LAYER (ft) DSL= 0.1  
 WEIGHT IN SURFACE LAYER (tons) WTSL= 1918.8  
 DEPTH OF NEW ACTIVE LAYER (ft) DSE= 0.0042  
 WEIGHT IN NEW ACTIVE LAYER(tons) WTMAL= 97.6  
 WEIGHT IN OLD ACTIVE LAYER(tons) WAL= 635.8  
 USEABLE WEIGHT, OLD INACTIVE LAYER WL= 226538.3  
 SURFACE AREA OF DEPOSIT (sq ft) SABK= 0.49516369E+06

\*\* INACTIVE LAYER \*\*

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0.009994     | 0.999449      | VF GRVL      | 0.025198      |
| F SAND                       | 0.069961     | 7.995595      | F GRVL       | 0.025198      |
| M SAND                       | 0.374794     | 45.474949     | M GRVL       | 0.005040      |
| C SAND                       | 0.374794     | 82.954303     | C GRVL       | 0.005040      |
| VC SAND                      | 0.104942     | 93.448522     | VC GRVL      | 0.005040      |

\*\* ACTIVE LAYER \*\*

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0.391813     | 39.181331     | VF GRVL      | 0.067850      |
| F SAND                       | 0.156193     | 54.800582     | F GRVL       | 0.075005      |
| M SAND                       | 0.263868     | 81.187410     | M GRVL       | 0.015090      |
| C SAND                       | 0.000000     | 81.187410     | C GRVL       | 0.015090      |
| VC SAND                      | 0.000000     | 81.187410     | VC GRVL      | 0.015090      |

C FINES, COEF(CFFML), MK POTENTIAL= 0.000000E+00 0.100000E+01 0.237600E+07  
 POTENTIAL TRANSPORT (tons/day): VF SAND 0.279192E+04 VF GRVL 0.108066E+01  
 F SAND 0.906230E+03 F GRVL 0.100000E-06  
 M SAND 0.533420E+03 M GRVL 0.100000E-06  
 C SAND 0.403607E+03 C GRVL 0.100000E-06  
 VC SAND 0.382254E+03 VC GRVL 0.100000E-06

| SEDIMENT OUTFLOW FROM SECTION NO. 32.000 |                 | GRAIN SIZE LOAD (tons/day)  |                 |
|--|-----------------|-----------------------------|-----------------|
| GRAIN SIZE                               | LOAD (tons/day) | GRAIN SIZE                  | LOAD (tons/day) |
| VERY FINE SAND. . . . .                  | 256.66          | VERY FINE GRAVEL. . . . .   | 0.04            |
| FINE SAND. . . . .                       | 78.38           | FINE GRAVEL. . . . .        | 0.00            |
| MEDIUM SAND. . . . .                     | 185.55          | MEDIUM GRAVEL. . . . .      | 0.00            |
| COARSE SAND. . . . .                     | 116.49          | COARSE GRAVEL. . . . .      | 0.00            |
| VERY COARSE SAND. . . . .                | 30.96           | VERY COARSE GRAVEL. . . . . | 0.00            |

Upstream of SECTION NO. 15.000 is . . .

| LOCAL INFLOW POINT # 1 | DISCHARGE (cfs) | SEDIMENT LOAD (tons/day) | TEMPERATURE (deg F) |
|------------------------|-----------------|--------------------------|---------------------|
| MAIN STEM INFLOW       | 1100.00         | 362.61                   | 64.05               |
| LOCAL INFLOW           | 150.00          | 14.45                    | 72.00               |
| TOTAL                  | 1250.00         | 377.06                   | 65.00               |

| SEDIMENT LOAD FROM LOCAL INFLOW |                 |                        |                 |
|---------------------------------|-----------------|------------------------|-----------------|
| GRAIN SIZE                      | LOAD (tons/day) | GRAIN SIZE             | LOAD (tons/day) |
| VERY FINE SAND. . . . .         | 6. 78           | VERY FINE GRAVEL. . .  | 0. 08           |
| FINE SAND. . . . .              | 4. 25           | FINE GRAVEL. . . . .   | 0. 03           |
| MEDIUM SAND. . . . .            | 2. 41           | MEDIUM GRAVEL. . . . . | 0. 00           |
| COARSE SAND. . . . .            | 0. 68           | COARSE GRAVEL. . . . . | 0. 00           |
| VERY COARSE SAND. . .           | 0. 21           | VERY COARSE GRAVEL     | 0. 00           |
|                                 |                 | TOTAL =                | 14. 45          |

FALL VELOCITIES - Method 2

|         | DIAMETER  | VELOCITY       | REY. NO.   | CD        |
|---------|-----------|----------------|------------|-----------|
| VF SAND | 0. 000290 | 0. 1931441E-01 | 0. 4941259 | 55. 02308 |
| F SAND  | 0. 000580 | 0. 5916114E-01 | 3. 027072  | 11. 72910 |
| M SAND  | 0. 001160 | 0. 1355164     | 13. 86779  | 4. 470784 |
| C SAND  | 0. 002320 | 0. 2833008     | 57. 98200  | 2. 045980 |
| VC SAND | 0. 004640 | 0. 4824925     | 197. 4999  | 1. 410740 |
| VF GRVL | 0. 009280 | 0. 7200893     | 589. 5120  | 1. 266733 |
| F GRVL  | 0. 018559 | 1. 040325      | 1703. 352  | 1. 213806 |
| M GRVL  | 0. 037118 | 1. 472894      | 4823. 231  | 1. 211086 |
| C GRVL  | 0. 074237 | 2. 082985      | 13642. 13  | 1. 211086 |
| VC GRVL | 0. 148474 | 2. 945788      | 38585. 85  | 1. 211086 |

\*\*\*\*\*  
TRACE OUTPUT FOR SECTION NO. 15. 000

HYDRAULIC PARAMETERS:

| VEL    | SLO       | EFD    | EFW      | N-VALUE | TAU      | USTARM   | FROUDE NO. |
|--------|-----------|--------|----------|---------|----------|----------|------------|
| 2. 137 | 0. 000485 | 6. 241 | 112. 022 | 0. 0450 | 0. 18889 | 0. 31196 | 0. 151     |

BED SEDIMENT CONTROL VOLUME COMPUTATIONS:

| NEW SURFACE AREA (SQ FT): | TOTAL      | K-PORTION  | S-PORTION |
|---------------------------|------------|------------|-----------|
|                           | 543327. 92 | 543327. 92 | 0. 00     |

GRADATION OF ACTIVE PLUS INACTIVE DEPOSITS

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0. 010618    | 1. 061792     | VF GRVL      | 0. 045645     |
| F SAND                       | 0. 070017    | 8. 063516     | F GRVL       | 0. 034096     |
| M SAND                       | 0. 325449    | 40. 608371    | M GRVL       | 0. 010834     |
| C SAND                       | 0. 365690    | 77. 177345    | C GRVL       | 0. 022336     |
| VC SAND                      | 0. 113092    | 88. 486534    | VC GRVL      | 0. 002223     |

SAND  
\*\* ARMOR LAYER \*\*  
STABILITY COEFFICIENT= 0. 78731  
MN. GRAIN DIAM = 0. 002878  
BED SURFACE EXPOSED = 0. 00000

|       | INACTIVE LAYER % | INACTIVE LAYER DEPTH | ACTIVE LAYER % | ACTIVE LAYER DEPTH |
|-------|------------------|----------------------|----------------|--------------------|
| CLAY  | 0. 0000          | 0. 00                | 0. 0000        | 0. 00              |
| SILT  | 0. 0000          | 0. 00                | 0. 0000        | 0. 00              |
| SAND  | 1. 0000          | 9. 64                | 1. 0000        | 0. 17              |
| TOTAL | 1. 0000          | 9. 64                | 1. 0000        | 0. 17              |

AVG. UNIT WEIGHT 0. 046500  
AVG. UNIT WEIGHT 0. 046500

COMPOSITE UNIT WT OF ACTIVE LAYER (t/cf)= 0. 046500  
COMPOSITE UNIT WT OF INACTIVE LAYER (t/cf)= 0. 046500  
DEPTH OF SURFACE LAYER (ft) DSL= 0. 1  
WEIGHT IN SURFACE LAYER (tons) WISL= 2105. 4  
DEPTH OF NEW ACTIVE LAYER (ft) DSE= 0. 0000  
WEIGHT IN NEW ACTIVE LAYER(tons) WTMKAL= 0. 0  
WEIGHT IN OLD ACTIVE LAYER(tons) WAL= 4252. 7  
USEABLE WEIGHT, OLD INACTIVE LAYER WL= 243631. 1  
SURFACE AREA OF DEPOSIT (sq ft) SABK= 0. 54332792E+06

\*\* INACTIVE LAYER \*\*

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0. 010000    | 1. 000000     | VF GRVL      | 0. 044734     |
| F SAND                       | 0. 070000    | 8. 000000     | F GRVL       | 0. 033457     |
| M SAND                       | 0. 327074    | 40. 707446    | M GRVL       | 0. 010638     |
| C SAND                       | 0. 366543    | 77. 361700    | C GRVL       | 0. 021915     |
| VC SAND                      | 0. 113457    | 88. 707445    | VC GRVL      | 0. 002181     |

\*\* ACTIVE LAYER \*\*

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0. 046017    | 4. 601728     | VF GRVL      | 0. 097841     |
| F SAND                       | 0. 071005    | 11. 702227    | F GRVL       | 0. 070689     |
| M SAND                       | 0. 232303    | 34. 932536    | M GRVL       | 0. 022074     |
| C SAND                       | 0. 316834    | 66. 615964    | C GRVL       | 0. 046463     |
| VC SAND                      | 0. 092150    | 75. 831001    | VC GRVL      | 0. 004624     |

C FINES, COEF(CFFML), MK POTENTIAL= 0. 000000E+00 0. 100000E+01 0. 270000E+07  
POTENTIAL TRANSPORT (tons/day): VF SAND 0. 326022E+04 VF GRVL 0. 230126E+01  
F SAND 0. 107158E+04 F GRVL 0. 328571E-03  
M SAND 0. 638850E+03 M GRVL 0. 100000E-06  
C SAND 0. 495316E+03 C GRVL 0. 100000E-06  
VC SAND 0. 491224E+03 VC GRVL 0. 100000E-06



| SEDIMENT OUTFLOW FROM SECTION NO. 15.000 |                 | 15.000                    |                 |
|--|-----------------|---------------------------|-----------------|
| GRAIN SIZE                               | LOAD (tons/day) | GRAIN SIZE                | LOAD (tons/day) |
| VERY FINE SAND. . . . .                  | 138.47          | VERY FINE GRAVEL. . . . . | 0.18            |
| FINE SAND. . . . .                       | 75.72           | FINE GRAVEL. . . . .      | 0.00            |
| MEDIUM SAND. . . . .                     | 168.18          | MEDIUM GRAVEL. . . . .    | 0.00            |
| COARSE SAND. . . . .                     | 162.61          | COARSE GRAVEL. . . . .    | 0.00            |
| VERY COARSE SAND. . . . .                | 47.90           | VERY COARSE GRAVEL        | 0.00            |

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
 EXAMPLE PROBLEM NO 3. MOVABLE BED  
 ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```

*****
TIME      ENTRY *      SAND *
DAYS     POINT *      OUTFLOW TRAP EFF *
53.00    58.000 *      13.25 *
          53.000 *      16.13 *
          42.000 *      0.36 *
TOTAL=   35.000 *      29.74      5.52      0.81 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      OUTFLOW TRAP EFF *
53.00    35.000 *      5.52 *
          33.000 *      5.52      1.54      0.72 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      OUTFLOW TRAP EFF *
53.00    33.000 *      1.54 *
          15.000 *      1.00 *
TOTAL=   1.000 *      2.54      0.07      0.97 *
*****
    
```

TABLE SB-1: SEDIMENT LOAD PASSING THE BOUNDARIES OF STREAM SEGMENT # 1

| SEDIMENT INFLOW at the Upstream Boundary: |                 |                           |                 |
|---|-----------------|---------------------------|-----------------|
| GRAIN SIZE                                | LOAD (tons/day) | GRAIN SIZE                | LOAD (tons/day) |
| VERY FINE SAND. . . . .                   | 66.90           | VERY FINE GRAVEL. . . . . | 0.00            |
| FINE SAND. . . . .                        | 53.32           | FINE GRAVEL. . . . .      | 0.00            |
| MEDIUM SAND. . . . .                      | 29.58           | MEDIUM GRAVEL. . . . .    | 0.00            |
| COARSE SAND. . . . .                      | 0.01            | COARSE GRAVEL. . . . .    | 0.00            |
| VERY COARSE SAND. . . . .                 | 0.00            | VERY COARSE GRAVEL        | 0.00            |
|   |                 |                           | TOTAL = 149.81  |

| SEDIMENT OUTFLOW from the Downstream Boundary |                 |                           |                 |
|---|-----------------|---------------------------|-----------------|
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE                | LOAD (tons/day) |
| VERY FINE SAND. . . . .                       | 2.05            | VERY FINE GRAVEL. . . . . | 0.00            |
| FINE SAND. . . . .                            | 1.13            | FINE GRAVEL. . . . .      | 0.00            |
| MEDIUM SAND. . . . .                          | 2.94            | MEDIUM GRAVEL. . . . .    | 0.00            |
| COARSE SAND. . . . .                          | 2.79            | COARSE GRAVEL. . . . .    | 0.00            |
| VERY COARSE SAND. . . . .                     | 1.08            | VERY COARSE GRAVEL        | 0.00            |
|   |                 |                           | TOTAL = 9.99    |

TABLE SB-2: STATUS OF THE BED PROFILE AT TIME = 53.000 DAYS

| SECTION NUMBER | BED CHANGE (ft) | WS ELEV (ft) | THALWEG (ft) | Q (cfs) | TRANSPORT RATE (tons/day) |
|----------------|-----------------|--------------|--------------|---------|---------------------------|
| 58.000         | -0.83           | 979.94       | 974.57       | 682.    | 818.                      |
| 55.000         | 0.04            | 979.11       | 972.94       | 682.    | 1476.                     |
| 53.000         | 0.25            | 975.42       | 972.45       | 1022.   | 4056.                     |
| 44.000         | 0.19            | 974.82       | 967.29       | 1022.   | 560.                      |
| 42.000         | 0.94            | 974.43       | 970.74       | 1100.   | 15.                       |
| 35.000         | 0.17            | 974.00       | 963.47       | 1100.   | 6.                        |
| 33.900         | 0.48            | 966.96       | 963.13       | 1100.   | 528.                      |
| 33.300         | 0.13            | 966.48       | 962.62       | 1100.   | 442.                      |
| 33.000         | 0.36            | 966.00       | 961.36       | 1100.   | 156.                      |
| 32.100         | -0.20           | 964.81       | 956.30       | 1100.   | 208.                      |
| 32.000         | -0.15           | 963.90       | 956.35       | 1100.   | 668.                      |
| 15.000         | -0.19           | 960.48       | 953.51       | 1250.   | 593.                      |
| 1.000          | 1.07            | 960.00       | 945.77       | 1250.   | 10.                       |

Accumulated Water Discharge from day zero (sfd)  
 MAIN  
 127750.00

SPRT A  
 ...Selective Printout Option  
 A - Print at all cross sections

=====

TIME STEP # 4  
 Q B FLOW 4 = BASE FLOW OF 750 CFS

-----

EXAMPLE PROBLEM NO 3. MOVABLE BED  
 ACCUMULATED TIME (yrs).... 0.148  
 FLOW DURATION (days)..... 1.000

UPSTREAM BOUNDARY CONDITIONS

| Stream Segment # 1<br>Section No. 58.000       | DISCHARGE<br>(cfs) | SEDIMENT LOAD<br>(tons/day) | TEMPERATURE<br>(deg F) |
|--|--------------------|-----------------------------|------------------------|
| INFLOW   | 532.00             | 93.30                       | 63.44                  |
| Upstream of SECTION NO. LOCAL INFLOW POINT # 3 |                    |                             |                        |
| 53.000 is...<br>DISCHARGE                      |                    |                             |                        |
|  | DISCHARGE<br>(cfs) | SEDIMENT LOAD<br>(tons/day) | TEMPERATURE<br>(deg F) |
| MAIN STEM INFLOW                               | 532.00             | 93.30                       | 63.44                  |
| LOCAL INFLOW                                   | 128.00             | 43.20                       | 67.00                  |
| TOTAL  | 660.00             | 136.50                      | 64.13                  |
| Upstream of SECTION NO. LOCAL INFLOW POINT # 2 |                    |                             |                        |
| 42.000 is...<br>DISCHARGE                      |                    |                             |                        |
|  | DISCHARGE<br>(cfs) | SEDIMENT LOAD<br>(tons/day) | TEMPERATURE<br>(deg F) |
| MAIN STEM INFLOW                               | 660.00             | 136.50                      | 64.13                  |
| LOCAL INFLOW                                   | 29.00              | 1.22                        | 70.00                  |
| TOTAL  | 689.00             | 137.72                      | 64.38                  |
| Upstream of SECTION NO. LOCAL INFLOW POINT # 1 |                    |                             |                        |
| 15.000 is...<br>DISCHARGE                      |                    |                             |                        |
|  | DISCHARGE<br>(cfs) | SEDIMENT LOAD<br>(tons/day) | TEMPERATURE<br>(deg F) |
| MAIN STEM INFLOW                               | 689.00             | 137.72                      | 64.38                  |
| LOCAL INFLOW                                   | 61.00              | 4.32                        | 72.00                  |
| TOTAL  | 750.00             | 142.04                      | 65.00                  |

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
EXAMPLE PROBLEM NO 3. MOVABLE BED  
ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```

*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
54.00    58.000 *      13.29          *
          53.000 *      16.15          *
          42.000 *      0.36           *
TOTAL=   35.000 *      29.81      5.52      0.81 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
54.00    35.000 *      5.52          *
TOTAL=   33.000 *      5.52      2.04      0.63 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW  TRAP EFF *
54.00    33.000 *      2.04          *
          15.000 *      1.00          *
TOTAL=   1.000 *      3.04      0.08      0.97 *
*****
    
```

TABLE SB-1: SEDIMENT LOAD PASSING THE BOUNDARIES OF STREAM SEGMENT # 1

| SEDIMENT INFLOW at the Upstream Boundary:     |                 |                    |                 |
|---|-----------------|--------------------|-----------------|
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |
| VERY FINE SAND...                             | 38.08           | VERY FINE GRAVEL.. | 0.00            |
| FINE SAND.....                                | 34.16           | FINE GRAVEL.....   | 0.00            |
| MEDIUM SAND.....                              | 21.06           | MEDIUM GRAVEL....  | 0.00            |
| COARSE SAND.....                              | 0.00            | COARSE GRAVEL....  | 0.00            |
| VERY COARSE SAND..                            | 0.00            | VERY COARSE GRAVEL | 0.00            |
|   |                 |                    | TOTAL = 93.30   |
| SEDIMENT OUTFLOW from the Downstream Boundary |                 |                    |                 |
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |
| VERY FINE SAND...                             | 6.28            | VERY FINE GRAVEL.. | 0.15            |
| FINE SAND.....                                | 2.82            | FINE GRAVEL.....   | 0.19            |
| MEDIUM SAND.....                              | 6.67            | MEDIUM GRAVEL....  | 0.07            |
| COARSE SAND.....                              | 6.38            | COARSE GRAVEL....  | 0.00            |
| VERY COARSE SAND..                            | 2.69            | VERY COARSE GRAVEL | 0.00            |
|   |                 |                    | TOTAL = 25.24   |

TABLE SB-2: STATUS OF THE BED PROFILE AT TIME = 54.000 DAYS

| SECTION NUMBER | BED CHANGE (ft) | WS ELEV (ft) | THALWEG (ft) | Q (cfs) | TRANSPORT RATE (tons/day) SAND |
|----------------|-----------------|--------------|--------------|---------|--------------------------------|
| 58.000         | -0.94           | 979.24       | 974.46       | 532.    | 415.                           |
| 55.000         | 0.00            | 978.47       | 972.90       | 532.    | 833.                           |
| 53.000         | 0.23            | 974.73       | 972.43       | 660.    | 1274.                          |
| 44.000         | 0.22            | 974.40       | 967.32       | 660.    | 138.                           |
| 42.000         | 0.94            | 974.18       | 970.74       | 689.    | 1.                             |
| 35.000         | 0.17            | 974.00       | 963.47       | 689.    | 0.                             |
| 33.900         | 0.40            | 965.77       | 963.05       | 689.    | 433.                           |
| 33.300         | 0.11            | 965.05       | 962.60       | 689.    | 713.                           |
| 33.000         | 0.33            | 963.74       | 961.33       | 689.    | 1000.                          |

|        |       |        |        |      |       |
|--------|-------|--------|--------|------|-------|
| 32.100 | -0.10 | 963.74 | 956.40 | 689. | 49.   |
| 32.000 | -0.18 | 963.13 | 956.32 | 689. | 694.  |
| 15.000 | -0.24 | 957.66 | 953.46 | 750. | 1530. |
| 1.000  | 1.22  | 957.00 | 945.92 | 750. | 25.   |

-----  
SSEND

0 DATA ERRORS DETECTED.

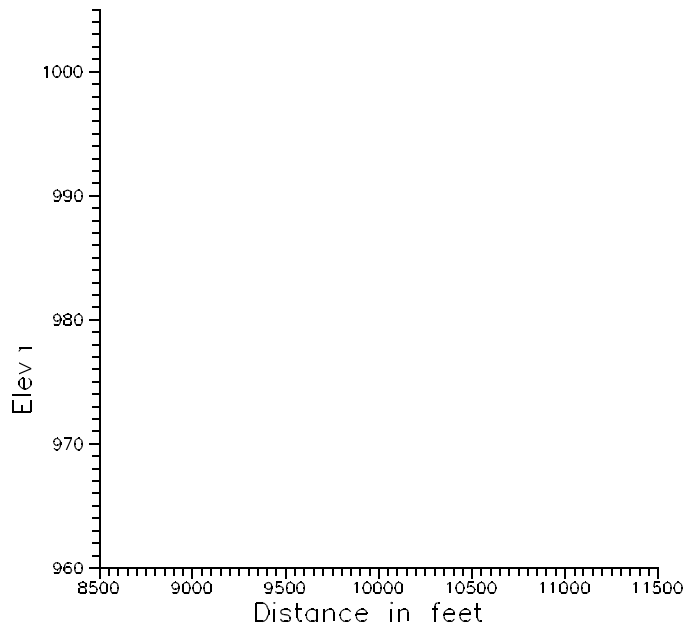
TOTAL NO. OF TIME STEPS READ = 4

TOTAL NO. OF WS PROFILES = 4

ITERATIONS IN EXNER EQ = 260

COMPUTATIONS COMPLETED

RUN TIME = 0 HOURS, 0 MINUTES & 2.00 SECONDS



|   |        |        |         |         |        |        |        |        |        |        |
|---|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| NV  | 22     | .045   | 965.6   | .064    | 988.8  |        |        |        |        |        |
| NV  | 12     | .08    | 965.6   | .13     | 988.8  |        |        |        |        |        |
| NV  | 33     | .1     | 965.6   | .11     | 982.0  | .12    | 988.8  |        |        |        |
| X1  | 15.0   | 27     | 10665.  | 10850.  | 3560.  | 3030.  | 3280.  |        |        |        |
| X3  |        |        |         | 10700.  | 961.0  | 11000. | 970.0  |        |        |        |
| GR  | 992.0  | 9570.  | 982.0   | 10110.  | 976.0  | 10300. | 976.0  | 10490. | 966.0  | 10610. |
| GR  | 964.7  | 10665. | 956.0   | 10673.  | 953.0  | 10693. | 954.0  | 10703. | 955.6  | 10723. |
| GR  | 958.6  | 10750. | 959.3   | 10800.  | 957.0  | 10822. | 957.3  | 10825. | 961.5  | 10850. |
| GR  | 962.0  | 10852. | 964.0   | 10970.  | 966.0  | 11015. | 961.0  | 11090. | 962.0  | 11150. |
| GR  | 970.0  | 11190. | 972.0   | 11310.  | 980.0  | 11410. | 984.0  | 11570. | 990.0  | 11770. |
| GR  | 990.0  | 11865. | 1000.0  | 12150.  |        |        |        |        |        |        |
| HD  | 15.0   | 10.    | 10673.  | 10852.  |        |        |        |        |        |        |
| CASCADE CREEK - Local Inflow  |        |        |         |         |        |        |        |        |        |        |
| QT  |        |        |         |         |        |        |        |        |        |        |
| NC  | .1     | .1     | .05     |         |        |        |        |        |        |        |
| X1  | 32.0   | 29     | 10057.0 | 10271.0 | 3630.  | 3060.  | 4240.  |        |        |        |
| GR  | 998.0  | 9080.  | 982.0   | 9250.   | 982.0  | 9510.  | 980.0  | 9600.  | 980.01 | 9925.  |
| GR  | 979.48 | 10000. | 978.5   | 10057.  | 968.6  | 10075. | 959.82 | 10087. | 956.5  | 10097. |
| GR  | 956.8  | 10117. | 957.8   | 10137.  | 959.4  | 10157. | 959.6  | 10177. | 959.8  | 10196. |
| GR  | 966.5  | 10225. | 971.2   | 10250.  | 978.5  | 10271. | 978.5  | 10300. | 978.6  | 10350. |
| GR  | 978.91 | 10370. | 978.96  | 10387.  | 980.0  | 10610. | 982.0  | 10745. | 982.0  | 11145. |
| GR  | 984.0  | 11150. | 992.0   | 11240.  | 1000.0 | 11330. | 1008.  | 11425. |        |        |
| HD  | 32.0   | 10.    | 10075.  | 10275.  |        |        |        |        |        |        |
| Section 32.1 is a duplicate of Sec 32.0 - Needed to model IBC at Sec 33.0 |        |        |         |         |        |        |        |        |        |        |
| X1  | 32.1   | 29     | 10057.0 | 10271.0 | 3130.  | 3250.  | 3320.  |        |        |        |
| X3  | 10     |        |         |         |        |        |        |        |        |        |
| GR  | 998.0  | 9080.  | 982.0   | 9250.   | 982.0  | 9510.  | 980.0  | 9600.  | 980.01 | 9925.  |
| GR  | 979.48 | 10000. | 978.5   | 10057.  | 968.6  | 10075. | 959.82 | 10087. | 956.5  | 10097. |
| GR  | 956.8  | 10117. | 957.8   | 10137.  | 959.4  | 10157. | 959.6  | 10177. | 959.8  | 10196. |
| GR  | 966.5  | 10225. | 971.2   | 10250.  | 978.5  | 10271. | 978.5  | 10300. | 978.6  | 10350. |
| GR  | 978.91 | 10370. | 978.96  | 10387.  | 980.0  | 10610. | 982.0  | 10745. | 982.0  | 11145. |
| GR  | 984.0  | 11150. | 992.0   | 11240.  | 1000.0 | 11330. | 1008.  | 11425. |        |        |
| HD  | 32.1   | 10.    | 10075.  | 10275.  |        |        |        |        |        |        |
| A spillway is located here.   |        |        |         |         |        |        |        |        |        |        |
| X1  | 33.0   | 21     | 1850.   | 2150.   | 0      | 0      | 0      |        |        |        |
| X5  |        |        |         | 2       |        |        |        |        |        |        |
| XL  |        |        | 250.    |         |        |        |        |        |        |        |
| GR  | 1000.  | 980.   | 990.0   | 1060.   | 980.0  | 1150.  | 982.0  | 1180.  | 982.0  | 1215.  |
| GR  | 980.0  | 1260.  | 982.0   | 1300.   | 982.0  | 1350.  | 980.0  | 1420.  | 980.0  | 1540.  |
| GR  | 982.0  | 1730.  | 982.0   | 1830.   | 984.41 | 1850.  | 979.19 | 1851.  | 961.0  | 1900.8 |
| GR  | 961.0  | 2099.2 | 976.0   | 2149.   | 984.5  | 2150.  | 982.0  | 2800.  | 990.0  | 3100.  |
| GR  | 1000.  | 3170.  |         |         |        |        |        |        |        |        |
| HD  | 33.0   | 0.     | 1851.   | 2149.   |        |        |        |        |        |        |
| Section 33.3 is a duplicate of Section 33.0.                              |        |        |         |         |        |        |        |        |        |        |
| X1  | 33.3   | 21     | 1850.   | 2150.   | 1550.  | 1750.  | 1750.  | .95    | 1.49   |        |
| XL  |        |        | 250.    |         |        |        |        |        |        |        |
| GR  | 1000.  | 980.   | 990.0   | 1060.   | 980.0  | 1150.  | 982.0  | 1180.  | 982.0  | 1215.  |
| GR  | 980.0  | 1260.  | 982.0   | 1300.   | 982.0  | 1350.  | 980.0  | 1420.  | 980.0  | 1540.  |
| GR  | 982.0  | 1730.  | 982.0   | 1830.   | 984.41 | 1850.  | 979.19 | 1851.  | 961.0  | 1900.8 |
| GR  | 961.0  | 2099.2 | 976.0   | 2149.   | 984.5  | 2150.  | 982.0  | 2800.  | 990.0  | 3100.  |
| GR  | 1000.  | 3170.  |         |         |        |        |        |        |        |        |
| HD  | 33.3   | 0.     | 1851.   | 2149.   |        |        |        |        |        |        |
| Section 33.9 is a duplicate of Sec 33.3 - Needed to model IBC at Sec 35.0 |        |        |         |         |        |        |        |        |        |        |
| X1  | 33.9   | 21     | 1850.   | 2150.   | 1050.  | 1050.  | 1050.  | .95    | 1.65   |        |
| X3  | 10     |        |         |         |        |        |        |        |        |        |
| GR  | 1000.  | 980.   | 990.0   | 1060.   | 980.0  | 1150.  | 982.0  | 1180.  | 982.0  | 1215.  |
| GR  | 980.0  | 1260.  | 982.0   | 1300.   | 982.0  | 1350.  | 980.0  | 1420.  | 980.0  | 1540.  |
| GR  | 982.0  | 1730.  | 982.0   | 1830.   | 984.41 | 1850.  | 979.19 | 1851.  | 961.0  | 1900.8 |
| GR  | 961.0  | 2099.2 | 976.0   | 2149.   | 984.5  | 2150.  | 982.0  | 2800.  | 990.0  | 3100.  |
| GR  | 1000.  | 3170.  |         |         |        |        |        |        |        |        |
| HD  | 33.9   | 0.     | 1851.   | 2149.   |        |        |        |        |        |        |
| A weir is located here.   |        |        |         |         |        |        |        |        |        |        |
| X1  | 35.0   | 22     | 9894.   | 10245.  | 0      | 0      | 0      |        |        |        |
| X3  | 10     |        |         |         |        |        |        |        |        |        |
| X5  |        | 974.   | 0.5     |         |        |        |        |        |        |        |
| GR  | 984.0  | 9035.  | 980.0   | 9070.   | 978.0  | 9135.  | 980.0  | 9185.  | 982.0  | 9270.  |
| GR  | 980.0  | 9465.  | 981.7   | 9595.   | 983.7  | 9745.  | 984.7  | 9894.  | 963.4  | 9894.1 |
| GR  | 963.3  | 9954.  | 967.1   | 9974.   | 967.4  | 10004. | 968.2  | 10044. | 967.6  | 10054. |
| GR  | 973.4  | 10115. | 977.4   | 10120.  | 983.7  | 10155. | 984.0  | 10245. | 982.0  | 10695. |
| GR  | 982.0  | 10895. | 1004.0  | 11085.  |        |        |        |        |        |        |
| HD  | 35.0   | 0.     | 9954.   | 10155.  |        | 969.0  | 9894.  | 9954.  |        | 1.0    |
| SILVER LAKE - - -   |        |        |         |         |        |        |        |        |        |        |
| NC  | .06    | .06    | .045    |         |        |        |        |        |        |        |
| X1  | 42.0   | 32     | 9880.   | 10130.  | 5370.  | 5000.  | 5210.  |        |        |        |
| GR  | 996.0  | 7130.  | 998.0   | 7310.   | 998.0  | 7930.  | 992.0  | 8205.  | 990.0  | 8495.  |
| GR  | 988.0  | 8780.  | 986.0   | 8990.   | 985.7  | 9570.  | 986.45 | 9707.  | 989.44 | 9857.  |
| GR  | 990.0  | 9880.  | 969.8   | 9881.   | 969.8  | 9941.  | 985.8  | 9941.  | 985.8  | 9943.  |
| GR  | 969.8  | 9943.  | 969.8   | 10001.  | 986.7  | 10001. | 986.7  | 10003. | 969.8  | 10003. |
| GR  | 969.8  | 10067. | 985.8   | 10067.  | 985.8  | 10069. | 969.8  | 10069. | 969.8  | 10129. |
| GR  | 989.9  | 10130. | 989.5   | 10180.  | 988.6  | 10230. | 987.6  | 10280. | 985.2  | 10430. |
| GR  | 986.8  | 11720. | 989.9   | 12310.  |        |        |        |        |        |        |
| HD  | 42.0   | 0.     | 9881.   | 10021.  |        | 971.0  | 9881.  | 9941.  |        | 1.0    |
| SILVER CREEK - Local Inflow   |        |        |         |         |        |        |        |        |        |        |
| QT  |        |        |         |         |        |        |        |        |        |        |
| X1  | 44.0   | 28     | 9845.   | 10127.  | 3200.  | 3800.  | 3500.  |        |        |        |
| XL  |        |        | 9850.   | 10200.  |        |        |        |        |        |        |

|          |        |        |        |        |        |       |        |        |        |
|----------|--------|--------|--------|--------|--------|-------|--------|--------|--------|
| GR 1002. | 8035.  | 992.0  | 8150.  | 990.0  | 8305.  | 990.0 | 8735.  | 988.0  | 8835.  |
| GR 996.0 | 9285.  | 1017.6 | 9425.  | 990.0  | 9505.  | 986.0 | 9650.  | 984.1  | 9788.  |
| GR 980.6 | 9845.  | 970.9  | 9868.  | 972.2  | 9898.  | 970.5 | 9968.  | 967.5  | 9998.  |
| GR 968.9 | 10028. | 967.4  | 10058. | 967.1  | 10078. | 971.9 | 10118. | 976.8  | 10127. |
| GR 977.8 | 10150. | 976.9  | 10193. | 982.0  | 10206. | 981.2 | 10300. | 979.2  | 10325. |
| GR 983.1 | 10400. | 999.8  | 10450. | 1002.4 | 10464. |       |        |        |        |
| HD 44.0  | 1.     | 9868.  | 10193. |        | 971.0  | 9968. | 10028. |        | 1.0    |
| X1 53.0  | 22     | 10000. | 10136. | 3366.  | 2832.  | 2942. |        |        |        |
| GR 1004. | 7550.  | 1000.0 | 7760.  | 998.0  | 8440.  | 996.0 | 8640.  | 996.0  | 8780.  |
| GR 994.0 | 8940.  | 986.0  | 9245.  | 986.3  | 9555.  | 986.3 | 9825.  | 983.8  | 9900.  |
| GR 982.8 | 10000. | 978.2  | 10011. | 974.0  | 10041. | 972.2 | 10071. | 972.6  | 10101. |
| GR 978.2 | 10121. | 988.7  | 10136. | 989.3  | 10154. | 999.2 | 10200. | 1000.1 | 10320. |
| GR 1002. | 10470. | 1004.0 | 10700. |        |        |       |        |        |        |
| HD 53.0  | 10.    | 10000. | 10136. |        |        |       |        |        |        |

BEAR CREEK - Local Inflow

|          |        |        |        |        |        |       |        |       |        |
|----------|--------|--------|--------|--------|--------|-------|--------|-------|--------|
| QT       |        |        |        |        |        |       |        |       |        |
| X1 55.0  | 18     | 9931.  | 10062. | 2275.  | 3430.  | 2770. |        |       |        |
| GR 1004. | 7592.  | 1000.0 | 7947.  | 996.0  | 8627.  | 990.0 | 9052.  | 986.0 | 9337.  |
| GR 984.3 | 9737.  | 984.7  | 9837.  | 985.5  | 9910.  | 987.2 | 9931.  | 978.1 | 9955.  |
| GR 974.8 | 9975.  | 974.2  | 10005. | 972.9  | 10035. | 973.2 | 10045. | 983.8 | 10062. |
| GR 985.8 | 10187. | 986.0  | 10307. | 990.0  | 10497. |       |        |       |        |
| HD 55.0  | 10.    | 9931.  | 10062. |        |        |       |        |       |        |
| X1 58.0  | 22     | 9912.  | 10015. | 1098.  | 1012.  | 1462. |        |       |        |
| GR 1006. | 8542.  | 1004.0 | 8952.  | 1000.0 | 9702.  | 997.2 | 9812.  | 996.3 | 9912.  |
| GR 976.2 | 9944.  | 975.4  | 9974.  | 978.2  | 9991.  | 990.4 | 10015. | 988.3 | 10062. |
| GR 988.8 | 10065. | 988.3  | 10065. | 989.3  | 10169. | 990.0 | 10172. | 992.0 | 10242. |
| GR 992.0 | 10492. | 988.0  | 10642. | 986.7  | 10852. | 988.0 | 11022. | 986.0 | 11097. |
| GR 986.0 | 11137. | 988.0  | 11192. |        |        |       |        |       |        |
| HD 58.0  | 3.4    | 9912.  | 10015. |        |        |       |        |       |        |

EJ South Fork, Zumbro River - Stream Segment 1 \*\* Example Problem 4 \*\*

T5 LOAD CURVE FROM GAGE DATA.

T6 BED GRADATIONS FROM FIELD SAMPLES.

T7 FULL RANGE OF SANDS AND GRAVELS

T8 SEDIMENT TRANSPORT BY YANG'S STREAM POWER [REF-ASCE JOURNAL (YANG 1971)]

|          |       |       |      |      |       |        |      |      |      |
|----------|-------|-------|------|------|-------|--------|------|------|------|
| I1       |       | 5     |      |      |       |        |      |      |      |
| I4 SAND  |       | 4     | 1    | 10   |       |        |      |      |      |
| I5       |       | .5    | .5   | .25  | .5    | .25    | 0    | 1.0  |      |
| LQ       |       | 1     | 50   | 1000 | 5800  | 90000  |      |      |      |
| LT TOTAL | .0110 |       | 1.5  | 320  | 4500. | 400000 |      |      |      |
| LF VFS   | .119  | .119  | .498 | .511 | .582  |        |      |      |      |
| LF FS    | .328  | .328  | .331 | .306 | .280  |        |      |      |      |
| LF MS    | .553  | .553  | .156 | .154 | .110  |        |      |      |      |
| LF CS    | .000  | .000  | .011 | .016 | .020  |        |      |      |      |
| LF VCS   | .000  | .000  | .004 | .008 | .005  |        |      |      |      |
| LF VFG   | .000  | .000  | .000 | .004 | .002  |        |      |      |      |
| LF FG    | .000  | .000  | .000 | .001 | .001  |        |      |      |      |
| LF MG    | .000  | .000  | .000 | .000 | .000  |        |      |      |      |
| LF CG    | .000  | .000  | .000 | .000 | .000  |        |      |      |      |
| LF VCG   | .0    | .0    | .000 | .000 | .000  |        |      |      |      |
| PF EXAMP | 1.0   | 1.0   | 32.0 | 16.0 | 96.5  | 8.0    | 95.0 | 4.0  | 91.0 |
| PFC 2.0  | 85.0  | 1.0   | 73.0 | .5   | 37.0  | .25    | 8.0  | .125 | 1.0  |
| PFC.0625 | 0.0   |       |      |      |       |        |      |      |      |
| PF EXAMP | 32.0  | 1.0   | 64.0 | 32.0 | 99.5  | 16.0   | 99.0 | 8.0  | 98.5 |
| PFC 4.0  | 96.0  | 2.0   | 93.5 | 1.0  | 83.0  | .50    | 45.5 | .250 | 8.0  |
| PFC .125 | 1.0   | .0625 | 0.0  |      |       |        |      |      |      |
| PF EXAMP | 58.0  | 1.0   | 64.0 | 32.0 | 97.0  | 16.0   | 94.0 | 8.0  | 94.0 |
| PFC 4.0  | 90.0  | 2.0   | 79.0 | 1.0  | 56.0  | .50    | 4.0  | .125 | 0.0  |

SLOCAL

LOAD TABLE - CASCADE CREEK - A LOCAL INFLOW

|          |       |       |       |       |       |  |  |  |  |
|----------|-------|-------|-------|-------|-------|--|--|--|--|
| LQL      |       | 1     | 100   | 1000  | 10000 |  |  |  |  |
| LTLTOTAL | .0040 |       | 10    | 500   | 30000 |  |  |  |  |
| LFL VFS  | .664  | .664  | .015  | .198  |       |  |  |  |  |
| LFL FS   | .207  | .207  | .245  | .181  |       |  |  |  |  |
| LFL MS   | .086  | .086  | .605  | .107  |       |  |  |  |  |
| LFL CS   | .031  | .031  | .052  | .098  |       |  |  |  |  |
| LFL VCS  | .008  | .008  | .039  | .127  |       |  |  |  |  |
| LFL VFG  | .0030 | .0030 | .0200 | .1160 |       |  |  |  |  |
| LFL FG   | .0010 | .0010 | .0110 | .0910 |       |  |  |  |  |
| LFL MG   | .0000 | .0000 | .0110 | .0530 |       |  |  |  |  |
| LFL CG   | .0000 | .0000 | .0000 | .0220 |       |  |  |  |  |
| LFL VCG  | .0000 | .0000 | .0000 | .0060 |       |  |  |  |  |

LOAD TABLE - SILVER CREEK - A LOCAL INFLOW

|          |       |       |       |       |       |  |  |  |  |
|----------|-------|-------|-------|-------|-------|--|--|--|--|
| LQL      |       | 1     | 100   | 1000  | 10000 |  |  |  |  |
| LTLTOTAL | .0040 |       | 10    | 500   | 30000 |  |  |  |  |
| LFL VFS  | .664  | .664  | .015  | .198  |       |  |  |  |  |
| LFL FS   | .207  | .207  | .245  | .181  |       |  |  |  |  |
| LFL MS   | .086  | .086  | .605  | .107  |       |  |  |  |  |
| LFL CS   | .031  | .031  | .052  | .098  |       |  |  |  |  |
| LFL VCS  | .008  | .008  | .039  | .127  |       |  |  |  |  |
| LFL VFG  | .0030 | .0030 | .0200 | .1160 |       |  |  |  |  |
| LFL FG   | .0010 | .0010 | .0110 | .0910 |       |  |  |  |  |
| LFL MG   | .0000 | .0000 | .0110 | .0530 |       |  |  |  |  |
| LFL CG   | .0000 | .0000 | .0000 | .0220 |       |  |  |  |  |
| LFL VCG  | .0000 | .0000 | .0000 | .0060 |       |  |  |  |  |

## LOAD TABLE - BEAR CREEK - A LOCAL INFLOW

|          |       |       |       |       |        |
|----------|-------|-------|-------|-------|--------|
| LQ       | 1.    | 100.  | 500.  | 1000. | 30000. |
| LTLTOTAL | .0020 | 30.0  | 500.  | 1200  | 22500  |
| LFL VFS  | .201  | .201  | .078  | .078  | .137   |
| LFL FS   | .342  | .342  | .172  | .175  | .218   |
| LFL MS   | .451  | .451  | .454  | .601  | .476   |
| LFL CS   | .001  | .001  | .197  | .142  | .158   |
| LFL VCS  | .000  | .000  | .000  | .003  | .008   |
| LFL VFG  | .0000 | .0000 | .0000 | .0000 | .0020  |
| LFL FG   | .0000 | .000  | .0000 | .0000 | .0010  |
| LFL MG   | .0000 | .000  | .0000 | .0000 | .0000  |
| LFL CG   | .0000 | .000  | .0000 | .0000 | .0000  |
| LFL VCG  | .0000 | .000  | .0000 | .0000 | .0000  |

SHYD

SB

2

SKL

Q A FLOW 1 = BASE FLOW OF 750 CFS

Q 750. 61. 29. 128.

R 956. 962.

T 65. 72. 70. 67.

W 2.

SDREDGE

Q B FLOW 2 = 50 DAYS AT BANK FULL DISCHARGE

Q 2500. 300. 150. 650.

R 965. 970.

X 2.5 50.

Q FLOW 3 = NEAR BANK FULL DISCHARGE

Q 1250. 150. 78. 340.

R 960. 966.

W 1.

SSED

NEW LOAD TABLE FOR MAIN STEM . .

|          |       |      |      |       |        |
|----------|-------|------|------|-------|--------|
| LPOINT   | 1     | 0    |      |       |        |
| LQ       | 1     | 50   | 1000 | 5800  | 90000  |
| LT TOTAL | .0110 | 1.5  | 320  | 4500. | 400000 |
| LF VFS   | .119  | .119 | .498 | .511  | .582   |
| LF FS    | .328  | .328 | .331 | .306  | .280   |
| LF MS    | .553  | .553 | .156 | .154  | .110   |
| LF CS    | .345  | .345 | .011 | .016  | .020   |
| LF VCS   | .025  | .025 | .004 | .008  | .005   |
| LF VFG   | .005  | .005 | .000 | .004  | .002   |
| LF FG    | .000  | .000 | .000 | .001  | .001   |
| LF MG    | .000  | .000 | .000 | .000  | .000   |
| LF CG    | .000  | .000 | .000 | .000  | .000   |
| LF VCG   | .0    | .0   | .000 | .000  | .000   |

NEW LOAD TABLE FOR SILVER CREEK - A LOCAL INFLOW

|          |       |       |       |       |  |  |  |  |  |
|----------|-------|-------|-------|-------|--|--|--|--|--|
| LPOINT   | 1     | 2     |       |       |  |  |  |  |  |
| LQ       | 1     | 100   | 1000  | 10000 |  |  |  |  |  |
| LTLTOTAL | .0040 | 10    | 500   | 30000 |  |  |  |  |  |
| LFL VFS  | .664  | .664  | .015  | .198  |  |  |  |  |  |
| LFL FS   | .207  | .207  | .245  | .181  |  |  |  |  |  |
| LFL MS   | .086  | .086  | .605  | .107  |  |  |  |  |  |
| LFL CS   | .031  | .031  | .052  | .098  |  |  |  |  |  |
| LFL VCS  | .008  | .008  | .039  | .127  |  |  |  |  |  |
| LFL VFG  | .0030 | .0030 | .0200 | .1160 |  |  |  |  |  |
| LFL FG   | .0010 | .0010 | .0110 | .0910 |  |  |  |  |  |
| LFL MG   | .0000 | .0000 | .0110 | .0530 |  |  |  |  |  |
| LFL CG   | .0000 | .0000 | .0000 | .0220 |  |  |  |  |  |
| LFL VCG  | .0000 | .0000 | .0000 | .0060 |  |  |  |  |  |

END

SRATING

|    |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| RC | 40    | 2000  | 0     | 0     | 950.0 | 955.1 | 958.0 | 960.0 | 962.0 |
| RC | 963.6 | 965.1 | 966.2 | 967.0 | 967.7 | 968.3 | 968.9 | 969.4 | 969.8 |
| RC | 970.2 | 970.6 | 971.0 | 971.4 | 971.8 | 972.1 | 972.4 | 972.7 | 972.9 |
| RC | 973.1 | 973.3 | 973.5 | 973.7 | 973.8 | 973.9 | 974.0 | 974.1 | 974.2 |
| RC | 974.3 | 974.4 | 974.5 | 974.6 | 974.7 | 974.8 | 974.9 | 975.0 |       |

SPRT

CP

1

PS

1.0 15.0

END

SNODREDGE

Q C FLOW 4 = BASE FLOW OF 750 CFS

Q 750. 61. 29. 128.

R 957. 963.

W 1.

SVOL A

SSEND

### 6.4.2 Transmissive Boundary Condition

With the addition of the SB record at the beginning of the hydrologic data, HEC-6 implements a transmissive boundary condition at each downstream boundary. This option causes all inflowing sediment to pass through the affected cross section without interacting with the bed. A caution: this option applies to all downstream boundaries in the model.

As in Example Problems 2 and 3, this example has two internal boundary conditions which effectively divide the model into 3 subreaches, each with its own downstream boundary.

The effect of the transmissive boundary condition on the 3 downstream boundaries can be seen by carefully reviewing the output of Example Problem 4. For instance, looking at TABLE SB-2 for the last time step, Sections 35.0, 33.0, and 1.0 all show that no bed change has occurred after a simulation of 52 days.

### 6.4.3 Limerinos' Bed Form Roughness Function

The Limerinos function (16) for bed form roughness is used in this example (\$KL record). The value of Manning's  $n$  resulting from this computation can be found in the "HYDRAULIC PARAMETERS" table of the C-level sediment output. For example, the  $n$  value calculated by the Limerinos equation for the last time step for Section No. 42.1 is 0.0153. Note, this computation overrides the roughness data (NC and NV records) in the geometric data.

### 6.4.4 Flow Duration Option

The use of X rather than W data to select the time step is also illustrated in this problem. This option allows a long period of constant flow to be subdivided into multiple computational time steps without repeating Q, Q, W data.

In this example, time step 2 represents 20 separate (incremental or computational) time steps each having a duration of 2.5 days. At the end of the last incremental time step, output is produced depicting the state of the river system for the last 2.5 day time step (i.e., instantaneous data such as the sediment load data in TABLE SB-2 are only for the last 2.5 day time step, while cumulative data, such as trap efficiency and bed change, represent changes since the start of the simulation.) Caution, because of this dichotomy, output produced by a time step such as this can be misleading. See Example Problem 7, Section 6.7.2.

### 6.4.5 Modifying the Sediment Load Tables

Sometimes the inflowing water vs. sediment relationship will change in time due to land use changes or even seasonal variations in vegetation. Such changes, should they be known or predicted, can be described in the flow data by using the SSED option. Example Problem 4 demonstrates the use of this option by changing the inflowing load curve for the main river and one local inflowing load curve prior to the last flow in the hydrograph. Tables echoing this data are shown in the output after time step 3.

### 6.4.6 Downstream Rating Curve

Prior to the last time step, a rating curve (\$RATING) was added to replace the stage hydrograph (R records). Although a rating curve is usually defined prior to the first time step, it can be placed (or replaced) before any time step of the simulation.



### 6.4.7 Accumulated Sediment Transported

Summary information regarding weight and volume of sediment can be requested via the A-level output option on the SVOL record. A-level output begins with the table labelled "SUMMARY TABLE: MASS AND VOLUME OF SEDIMENT". This table lists cumulative values of sediment transported through and deposited at each cross section since time zero. The difference between the sediment volume entering and leaving a cross section represents the material scoured from or deposited into the control volume associated with that cross section. This value is given under the heading "SEDIMENT DEPOSITED IN REACH IN CUBIC YARDS"; negative values represent scour. Under the heading "TOTAL SEDIMENT per grain size THROUGH EACH CROSS SECTION" are tables listing the total sediment transported through each cross section's control volume since the start of the simulation by grain size. Because the SPRT option was invoked to limit output to Sections 1.0 and 15.0, only tables for these cross sections have been produced.

Table 6-4b  
Example Problem 4 - Output  
Sediment Options

```

*****
* SCOUR AND DEPOSITION IN RIVERS AND RESERVOIRS *
* Version: 4.1.00 - AUGUST 1993 *
* INPUT FILE: example4.DAT *
* OUTPUT FILE: example4.OUT *
* RUN DATE: 31 AUG 93 RUN TIME: 16:06:03 *
*****

                X   X   XXXXXX   XXXXX   XXXXX
                X   X   X         X   X   X   X
                X   X   X         X   X   X   X
                XXXXXX   XXXX   X         XXXXX   XXXXXX
                X   X   X         X   X   X   X
                X   X   X         X   X   X   X
                X   X   XXXXXX   XXXXX   XXXXX

*****
* MAXIMUM LIMITS FOR THIS VERSION ARE: *
* 10 Stream Segments (Main Stem + Tributaries) *
* 150 Cross Sections *
* 100 Elevation/Station Points per Cross Section *
* 20 Grain Sizes *
* 10 Control Points *
*****

```

The output produced during processing of the geometry and sediment data does not differ from that produced for Example Problem 3. It has therefore been omitted from this table.  
Refer to Table 6-3b.

```

=====
SHYD
BEGIN COMPUTATIONS.
-----

```

```

SB          2
...Transmissive Boundary Condition - 0N
-----

```

```

SKL
...USING LIMERINOS METHOD TO CALCULATE BED ROUGHNESS.
=====

```

TIME STEP # 1  
 Q A FLOW 1 = BASE FLOW OF 750 CFS

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
 EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.  
 ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```

*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW TRAP EFF *
2.00     58.000 *      0.09   0.00    1.00 *
          53.000 *      0.04   0.00    1.00 *
          42.000 *      0.00   0.00    1.00 *
TOTAL=   35.000 *      0.14   0.00    1.00 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW TRAP EFF *
2.00     35.000 *      0.00   0.00    0.36 *
TOTAL=   33.000 *      0.00   0.00    0.36 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW TRAP EFF *
2.00     33.000 *      0.00   0.00    0.00 *
          15.000 *      0.00   0.00    0.00 *
TOTAL=   1.000 *      0.00   2.96  -692.13 *
*****
    
```

SDREDGE

STREAM SEGMENT # 1: EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.

SEC NO. 42.000  
 ELEVATION OF DREDGED CHANNEL INCLUDING 1.00 FEET OF OVER DREDGING= 970.00

=====

TIME STEP # 2  
 Q B FLOW 2 = 50 DAYS AT BANK FULL DISCHARGE  
 COMPUTING FROM TIME= 2.0000 DAYS TO TIME= 52.0000 DAYS IN 20 COMPUTATION STEPS

EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.  
 ACCUMULATED TIME (yrs).... 0.142  
 FLOW DURATION (days)..... 2.500

UPSTREAM BOUNDARY CONDITIONS

| Stream Segment #                               | DISCHARGE (cfs)              | SEDIMENT LOAD (tons/day) | TEMPERATURE (deg F) |
|--|------------------------------|--------------------------|---------------------|
| Section No. 58.000                             |                              |                          |                     |
| INFLOW   | 1400.00                      | 529.98                   | 62.04               |
| Upstream of SECTION NO. LOCAL INFLOW POINT # 3 | 53.000 is... DISCHARGE (cfs) | SEDIMENT LOAD (tons/day) | TEMPERATURE (deg F) |
| MAIN STEM INFLOW                               | 1400.00                      | 529.98                   | 62.04               |
| LOCAL INFLOW                                   | 650.00                       | 647.71                   | 67.00               |
| TOTAL  | 2050.00                      | 1177.69                  | 63.61               |
| Upstream of SECTION NO. LOCAL INFLOW POINT # 2 | 42.000 is... DISCHARGE (cfs) | SEDIMENT LOAD (tons/day) | TEMPERATURE (deg F) |
| MAIN STEM INFLOW                               | 2050.00                      | 1177.69                  | 63.61               |
| LOCAL INFLOW                                   | 150.00                       | 14.45                    | 70.00               |
| TOTAL  | 2200.00                      | 1192.13                  | 64.05               |
| Upstream of SECTION NO. LOCAL INFLOW POINT # 1 | 15.000 is... DISCHARGE (cfs) | SEDIMENT LOAD (tons/day) | TEMPERATURE (deg F) |
| MAIN STEM INFLOW                               | 2200.00                      | 1192.13                  | 64.05               |
| LOCAL INFLOW                                   | 300.00                       | 40.00                    | 72.00               |
| TOTAL  | 2500.00                      | 1232.13                  | 65.00               |

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
 EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.  
 ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```

*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW TRAP EFF *
52.00    58.000 *      13.17  2.05    0.93 *
          53.000 *      16.03  0.08    0.96 *
          42.000 *      0.36   0.00    0.00 *
TOTAL=   35.000 *      29.56  2.05    0.93 *
*****
TIME      ENTRY *      SAND *
DAYS     POINT *      INFLOW  OUTFLOW TRAP EFF *
52.00    35.000 *      2.05   0.08    0.96 *
TOTAL=   33.000 *      2.05   0.08    0.96 *
*****
TIME      ENTRY *      SAND *
    
```

|        |          |        |         |            |
|--------|----------|--------|---------|------------|
| DAYS   | POINT *  | INFLOW | OUTFLOW | TRAP EFF * |
| 52.00  | 33.000 * | 0.08   |         | *          |
|        | 15.000 * | 0.99   |         | *          |
| TOTAL= | 1.000 *  | 1.07   | 3.42    | -2.21 *    |

\*\*\*\*\*

TABLE SB-1: SEDIMENT LOAD PASSING THE BOUNDARIES OF STREAM SEGMENT # 1

| SEDIMENT INFLOW at the Upstream Boundary: |                 |                           |                 |
|---|-----------------|---------------------------|-----------------|
| GRAIN SIZE                                | LOAD (tons/day) | GRAIN SIZE                | LOAD (tons/day) |
| VERY FINE SAND. . . . .                   | 265.63          | VERY FINE GRAVEL. . . . . | 0.00            |
| FINE SAND. . . . .                        | 173.06          | FINE GRAVEL. . . . .      | 0.00            |
| MEDIUM SAND. . . . .                      | 82.59           | MEDIUM GRAVEL. . . . .    | 0.00            |
| COARSE SAND. . . . .                      | 6.27            | COARSE GRAVEL. . . . .    | 0.00            |
| VERY COARSE SAND. . . . .                 | 2.42            | VERY COARSE GRAVEL        | 0.00            |
|   |                 | TOTAL =                   | 529.98          |

| SEDIMENT OUTFLOW from the Downstream Boundary |                 |                           |                 |
|---|-----------------|---------------------------|-----------------|
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE                | LOAD (tons/day) |
| VERY FINE SAND. . . . .                       | 1.42            | VERY FINE GRAVEL. . . . . | 0.03            |
| FINE SAND. . . . .                            | 1.61            | FINE GRAVEL. . . . .      | 0.00            |
| MEDIUM SAND. . . . .                          | 7.44            | MEDIUM GRAVEL. . . . .    | 0.00            |
| COARSE SAND. . . . .                          | 9.01            | COARSE GRAVEL. . . . .    | 0.00            |
| VERY COARSE SAND. . . . .                     | 3.68            | VERY COARSE GRAVEL        | 0.00            |
|   |                 | TOTAL =                   | 23.18           |

TABLE SB-2: STATUS OF THE BED PROFILE AT TIME = 52.000 DAYS

| SECTION NUMBER | BED CHANGE (ft) | WS ELEV (ft) | THALWEG (ft) | Q (cfs) | TRANSPORT RATE (tons/day) SAND |
|----------------|-----------------|--------------|--------------|---------|--------------------------------|
| 58.000         | -2.79           | 978.33       | 972.61       | 1400.   | 577.                           |
| 55.000         | -1.24           | 978.30       | 971.66       | 1400.   | 837.                           |
| 53.000         | -1.55           | 976.02       | 970.65       | 2050.   | 1885.                          |
| 44.000         | 0.92            | 974.67       | 968.02       | 2050.   | 1258.                          |
| 42.000         | 1.75            | 974.19       | 971.55       | 2200.   | 138.                           |
| 35.000         | 0.00            | 974.00       | 963.30       | 2200.   | 138.                           |
| 33.900         | 0.69            | 970.03       | 963.34       | 2200.   | 9.                             |
| 33.300         | 0.01            | 970.01       | 962.50       | 2200.   | 4.                             |
| 33.000         | 0.00            | 970.00       | 961.00       | 2200.   | 4.                             |
| 32.100         | -0.52           | 965.75       | 955.98       | 2200.   | 107.                           |
| 32.000         | -0.05           | 965.23       | 956.45       | 2200.   | 138.                           |
| 15.000         | -0.18           | 964.99       | 953.52       | 2500.   | 23.                            |
| 1.000          | 0.00            | 965.00       | 944.70       | 2500.   | 23.                            |

STREAM SEGMENT # 1: EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.

|  |        |                             |        |
|--|--------|-----------------------------|--------|
| SEC NO.                                | 42.000 |                             |        |
| ELEVATION OF DREDGED CHANNEL INCLUDING |        | 1.00 FEET OF OVER DREDGING= | 970.00 |
| SEC NO.                                | 44.000 |                             |        |
| ELEVATION OF DREDGED CHANNEL INCLUDING |        | 1.00 FEET OF OVER DREDGING= | 970.00 |

|       |     |              |              |              |         |
|-------|-----|--------------|--------------|--------------|---------|
| LFL   | ME  | 0.100000E-19 | 0.100000E-19 | 5.50000      | 1590.00 |
| LFL   | CG  | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 660.000 |
| LFL   | VCG | 0.100000E-19 | 0.100000E-19 | 0.100000E-19 | 180.000 |
| TOTAL |     | 0.400000E-02 | 10.0000      | 499.000      | 29970.0 |

SRATING

| Downstream Boundary Condition - Rating Curve |         |           |           |         |           |
|--|---------|-----------|-----------|---------|-----------|
| Elevation                                    | Stage   | Discharge | Elevation | Stage   | Discharge |
| 950.000                                      | 950.000 | 0.000     | 972.400   | 972.400 | 40000.000 |
| 955.100                                      | 955.100 | 2000.000  | 972.700   | 972.700 | 42000.000 |
| 958.000                                      | 958.000 | 4000.000  | 972.900   | 972.900 | 44000.000 |
| 960.000                                      | 960.000 | 6000.000  | 973.100   | 973.100 | 46000.000 |
| 962.000                                      | 962.000 | 8000.000  | 973.300   | 973.300 | 48000.000 |
| 963.600                                      | 963.600 | 10000.000 | 973.500   | 973.500 | 50000.000 |
| 965.100                                      | 965.100 | 12000.000 | 973.700   | 973.700 | 52000.000 |
| 966.200                                      | 966.200 | 14000.000 | 973.800   | 973.800 | 54000.000 |
| 967.000                                      | 967.000 | 16000.000 | 973.900   | 973.900 | 56000.000 |
| 967.700                                      | 967.700 | 18000.000 | 974.000   | 974.000 | 58000.000 |
| 968.300                                      | 968.300 | 20000.000 | 974.100   | 974.100 | 60000.000 |
| 968.900                                      | 968.900 | 22000.000 | 974.200   | 974.200 | 62000.000 |
| 969.400                                      | 969.400 | 24000.000 | 974.300   | 974.300 | 64000.000 |
| 969.800                                      | 969.800 | 26000.000 | 974.400   | 974.400 | 66000.000 |
| 970.200                                      | 970.200 | 28000.000 | 974.500   | 974.500 | 68000.000 |
| 970.600                                      | 970.600 | 30000.000 | 974.600   | 974.600 | 70000.000 |
| 971.000                                      | 971.000 | 32000.000 | 974.700   | 974.700 | 72000.000 |
| 971.400                                      | 971.400 | 34000.000 | 974.800   | 974.800 | 74000.000 |
| 971.800                                      | 971.800 | 36000.000 | 974.900   | 974.900 | 76000.000 |
| 972.100                                      | 972.100 | 38000.000 | 975.000   | 975.000 | 78000.000 |

SPRT

... Selective Printout Option  
 - Print at the following cross sections  
 CP 1  
 PS 1.0 15.0  
 END

SNODREDGE

=====

TIME STEP # 4  
 Q C FLOW 4 = BASE FLOW OF 750 CFS

EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.  
 ACCUMULATED TIME (yrs).... 0.148  
 FLOW DURATION (days)..... 1.000

UPSTREAM BOUNDARY CONDITIONS

| Stream Segment # | DISCHARGE | SEDIMENT LOAD | TEMPERATURE |
|------------------|-----------|---------------|-------------|
| Section No.      | (cfs)     | (tons/day)    | (deg F)     |
| INFLOW           | 532.00    | 96.26         | 63.44       |

| SEDIMENT INFLOW at SECTION NO. 58.000 |                 |                    |                 |       |
|---------------------------------------|-----------------|--------------------|-----------------|-------|
| GRAIN SIZE                            | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |       |
| VERY FINE SAND....                    | 38.08           | VERY FINE GRAVEL.. | 0.00            |       |
| FINE SAND.....                        | 34.16           | FINE GRAVEL.....   | 0.00            |       |
| MEDIUM SAND.....                      | 21.06           | MEDIUM GRAVEL....  | 0.00            |       |
| COARSE SAND.....                      | 2.35            | COARSE GRAVEL....  | 0.00            |       |
| VERY COARSE SAND..                    | 0.61            | VERY COARSE GRAVEL | 0.00            |       |
|                                       |                 |                    | TOTAL =         | 96.26 |

FALL VELOCITIES - Method 2

|         | DIAMETER | VELOCITY      | REY. NO.  | CD       |
|---------|----------|---------------|-----------|----------|
| VF SAND | 0.000290 | 0.1895778E-01 | 0.4746927 | 57.11272 |
| F SAND  | 0.000580 | 0.5840962E-01 | 2.925091  | 12.03287 |
| M SAND  | 0.001160 | 0.1341560     | 13.43676  | 4.561910 |
| C SAND  | 0.002320 | 0.2818261     | 56.45410  | 2.067449 |
| VC SAND | 0.004640 | 0.4816294     | 192.9560  | 1.415800 |
| VF GRVL | 0.009280 | 0.7196122     | 576.5988  | 1.268414 |
| F GRVL  | 0.018559 | 1.040018      | 1666.653  | 1.214521 |
| M GRVL  | 0.037118 | 1.472894      | 4720.706  | 1.211086 |
| C GRVL  | 0.074237 | 2.082985      | 13352.15  | 1.211086 |
| VC GRVL | 0.148474 | 2.945788      | 37765.65  | 1.211086 |

| Upstream of SECTION NO.<br>LOCAL INFLOW POINT # 1 | 15.000 is...<br>DISCHARGE<br>(cfs) | SEDIMENT LOAD<br>(tons/day) | TEMPERATURE<br>(deg F) |
|---|------------------------------------|-----------------------------|------------------------|
| MAIN STEM INFLOW                                  | 689.00                             | 140.68                      | 64.38                  |
| LOCAL INFLOW                                      | 61.00                              | 4.32                        | 72.00                  |
| <b>TOTAL</b>                                      | <b>750.00</b>                      | <b>145.00</b>               | <b>65.00</b>           |

| SEDIMENT LOAD FROM LOCAL INFLOW: |                 |                    |                 |
|----------------------------------|-----------------|--------------------|-----------------|
| GRAIN SIZE                       | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |
| VERY FINE SAND...                | 2.87            | VERY FINE GRAVEL.. | 0.01            |
| FINE SAND.....                   | 0.89            | FINE GRAVEL.....   | 0.00            |
| MEDIUM SAND.....                 | 0.37            | MEDIUM GRAVEL..... | 0.00            |
| COARSE SAND.....                 | 0.13            | COARSE GRAVEL..... | 0.00            |
| VERY COARSE SAND..               | 0.03            | VERY COARSE GRAVEL | 0.00            |
|                                  |                 | <b>TOTAL =</b>     | <b>4.32</b>     |

| FALL VELOCITIES - Method 2 |          |               |           |          |
|----------------------------|----------|---------------|-----------|----------|
|                            | DIAMETER | VELOCITY      | REY. NO.  | CD       |
| VF SAND                    | 0.000290 | 0.1931441E-01 | 0.4941259 | 55.02308 |
| F SAND                     | 0.000580 | 0.5916114E-01 | 3.027072  | 11.72910 |
| M SAND                     | 0.001160 | 0.1355164     | 13.86779  | 4.470784 |
| C SAND                     | 0.002320 | 0.2833008     | 57.98200  | 2.045980 |
| VC SAND                    | 0.004640 | 0.4824925     | 197.4999  | 1.410740 |
| VF GRVL                    | 0.009280 | 0.7200893     | 589.5120  | 1.266733 |
| F GRVL                     | 0.018559 | 1.040325      | 1703.352  | 1.213806 |
| M GRVL                     | 0.037118 | 1.472894      | 4823.231  | 1.211086 |
| C GRVL                     | 0.074237 | 2.082985      | 13642.13  | 1.211086 |
| VC GRVL                    | 0.148474 | 2.945788      | 38585.85  | 1.211086 |

\*\*\*\*\*  
TRACE OUTPUT FOR SECTION NO. 15.000  
\*\*\*\*\*

| HYDRAULIC PARAMETERS: |          |       |        |         |         |         |            |
|-----------------------|----------|-------|--------|---------|---------|---------|------------|
| VEL                   | SLO      | EFD   | EFW    | N-VALUE | TAU     | USTARM  | FROUDE NO. |
| 4.382                 | 0.000558 | 4.555 | 72.960 | 0.0167  | 0.15863 | 0.28588 | 0.362      |

| BED SEDIMENT CONTROL VOLUME COMPUTATIONS: |           |           |           |
|---|-----------|-----------|-----------|
| NEW SURFACE AREA (SQ FT):                 | TOTAL     | K-PORTION | S-PORTION |
|   | 336901.25 | 336901.25 | 0.00      |

| GRADATION OF ACTIVE PLUS INACTIVE DEPOSITS |         |              |               |              |               |           |
|--|---------|--------------|---------------|--------------|---------------|-----------|
| BED MATERIAL PER GRAIN                     | SIZE:   | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |           |
|  | VF SAND | 0.010519     | 1.051939      | VF GRVL      | 0.045573      | 93.063185 |
|  | F SAND  | 0.068551     | 7.907044      | F GRVL       | 0.034049      | 96.468071 |
|  | M SAND  | 0.324948     | 40.401812     | M GRVL       | 0.010808      | 97.548838 |
|  | C SAND  | 0.367062     | 77.107991     | C GRVL       | 0.022292      | 99.777989 |
|  | VC SAND | 0.113979     | 88.505902     | VC GRVL      | 0.002220      | 99.999998 |

SAND  
\*\* ARMOR LAYER \*\*  
STABILITY COEFFICIENT= 0.80177  
MIN. GRAIN DIAM = 0.030569  
BED SURFACE EXPOSED = 0.00000

|       | INACTIVE LAYER |       | ACTIVE LAYER |       |
|-------|----------------|-------|--------------|-------|
|       | %              | DEPTH | %            | DEPTH |
| CLAY  | 0.0000         | 0.00  | 0.0000       | 0.00  |
| SILT  | 0.0000         | 0.00  | 0.0000       | 0.00  |
| SAND  | 1.0000         | 9.25  | 1.0000       | 0.57  |
| TOTAL | 1.0000         | 9.25  | 1.0000       | 0.57  |

| AVG. UNIT WEIGHT | AVG. UNIT WEIGHT |
|------------------|------------------|
| 0.046500         | 0.046500         |

COMPOSITE UNIT WT OF ACTIVE LAYER (t/cf)= 0.046500  
COMPOSITE UNIT WT OF INACTIVE LAYER (t/cf)= 0.046500  
DEPTH OF SURFACE LAYER (ft) DSL= 0.1  
WEIGHT IN SURFACE LAYER (tons) WTSL= 1305.5  
DEPTH OF NEW ACTIVE LAYER (ft) DSE= 0.0373  
WEIGHT IN NEW ACTIVE LAYER (tons) WTMAL= 584.9  
WEIGHT IN OLD ACTIVE LAYER (tons) WAL= 8927.8  
USEABLE WEIGHT, OLD INACTIVE LAYER WIL= 144962.8  
SURFACE AREA OF DEPOSIT (sq ft) SABK= 0.33690125E+06

| ** INACTIVE LAYER **   |         |              |               |              |               |           |
|------------------------|---------|--------------|---------------|--------------|---------------|-----------|
| BED MATERIAL PER GRAIN | SIZE:   | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |           |
|                        | VF SAND | 0.010000     | 1.000000      | VF GRVL      | 0.044734      | 93.180849 |
|                        | F SAND  | 0.070000     | 8.000000      | F GRVL       | 0.033457      | 96.526593 |
|                        | M SAND  | 0.327074     | 40.707446     | M GRVL       | 0.010638      | 97.590423 |
|                        | C SAND  | 0.366543     | 77.361700     | C GRVL       | 0.021915      | 99.781912 |
|                        | VC SAND | 0.113457     | 88.707445     | VC GRVL      | 0.002181      | 99.999998 |

| ** ACTIVE LAYER **     |         |              |               |              |               |           |
|------------------------|---------|--------------|---------------|--------------|---------------|-----------|
| BED MATERIAL PER GRAIN | SIZE:   | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |           |
|                        | VF SAND | 0.018953     | 1.895284      | VF GRVL      | 0.059193      | 91.152666 |
|                        | F SAND  | 0.045024     | 6.397700      | F GRVL       | 0.043652      | 95.517835 |
|                        | M SAND  | 0.290415     | 35.439182     | M GRVL       | 0.013558      | 96.873609 |

C SAND 0.375493 72.988468 C GRVL 0.028407 99.714290  
 VC SAND 0.122449 85.233411 VC GRVL 0.002857 100.000000

C FINES, COEF(CFFML), MK POTENTIAL= 0.000000E+00 0.100000E+01 0.162000E+07  
 POTENTIAL TRANSPORT (tons/day): VF SAND 0.767631E+04 VF GRVL 0.540007E+02  
 F SAND 0.222208E+04 F GRVL 0.856678E+02  
 M SAND 0.120096E+04 M GRVL 0.924255E+02  
 C SAND 0.879011E+03 C GRVL 0.343755E+01  
 VC SAND 0.885363E+03 VC GRVL 0.100000E-06

| BED MATERIAL PER GRAIN SIZE: | BED FRACTION | PERCENT FINER | BED FRACTION | PERCENT FINER |
|------------------------------|--------------|---------------|--------------|---------------|
| VF SAND                      | 0.011944     | 1.194380      | VF GRVL      | 0.064549      |
| F SAND                       | 0.037695     | 4.963900      | F GRVL       | 0.047476      |
| M SAND                       | 0.276179     | 32.581777     | M GRVL       | 0.014690      |
| C SAND                       | 0.387609     | 71.342665     | C GRVL       | 0.031077      |
| VC SAND                      | 0.125654     | 83.908024     | VC GRVL      | 0.003127      |

| SEDIMENT OUTFLOW FROM SECTION NO. 15.000 |        | GRAIN SIZE LOAD (tons/day) |      |
|--|--------|----------------------------|------|
| VERY FINE SAND...                        | 115.42 | VERY FINE GRAVEL..         | 3.19 |
| FINE SAND.....                           | 101.72 | FINE GRAVEL.....           | 3.74 |
| MEDIUM SAND.....                         | 348.91 | MEDIUM GRAVEL....          | 1.25 |
| COARSE SAND.....                         | 332.83 | COARSE GRAVEL....          | 0.10 |
| VERY COARSE SAND..                       | 108.39 | VERY COARSE GRAVEL         | 0.00 |

\*\*\*\*\*  
 TRACE OUTPUT FOR SECTION NO. 1.000  
 -----

HYDRAULIC PARAMETERS:  
 VEL SLO EFD EFW N-VALUE TAU USTARM FROUDE NO.  
 4.011 0.000004 5.838 83.730 0.0176 0.00159 0.02864 0.293

BED SEDIMENT CONTROL VOLUME COMPUTATIONS:  
 NEW SURFACE AREA (SQ FT): TOTAL 209373.61 K-PORITION 209373.61 S-PORITION 0.00

TRANSMISSIVE BOUNDARY CONDITION = TYPE 2  
 BED MATERIAL PER GRAIN SIZE: BED FRACTION PERCENT FINER BED FRACTION PERCENT FINER  
 VF SAND 0.010000 1.000000 VF GRVL 0.060000 90.999998  
 F SAND 0.070000 8.000000 F GRVL 0.040000 94.999998  
 M SAND 0.290000 36.999999 M GRVL 0.015000 96.499998  
 C SAND 0.360000 72.999998 C GRVL 0.035000 99.999998  
 VC SAND 0.120000 84.999998 VC GRVL 0.000000 99.999998

| SEDIMENT OUTFLOW FROM SECTION NO. 1.000 |        | GRAIN SIZE LOAD (tons/day) |      |
|---|--------|----------------------------|------|
| VERY FINE SAND...                       | 115.42 | VERY FINE GRAVEL..         | 3.19 |
| FINE SAND.....                          | 101.72 | FINE GRAVEL.....           | 3.74 |
| MEDIUM SAND.....                        | 348.91 | MEDIUM GRAVEL....          | 1.25 |
| COARSE SAND.....                        | 332.83 | COARSE GRAVEL....          | 0.10 |
| VERY COARSE SAND..                      | 108.39 | VERY COARSE GRAVEL         | 0.00 |

TABLE SA-1. TRAP EFFICIENCY ON STREAM SEGMENT # 1  
 EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.  
 ACCUMULATED AC-FT ENTERING AND LEAVING THIS STREAM SEGMENT

```
*****
TIME   ENTRY *   SAND *
DAYS   POINT *   INFLOW   OUTFLOW TRAP EFF *
54.00  58.000 *   13.30    2.05    0.93 *
      53.000 *   16.15    1.22    0.40 *
      42.000 *   0.36     0.00    0.00 *
TOTAL= 35.000 *   29.81    2.05    0.93 *
*****
TIME   ENTRY *   SAND *
DAYS   POINT *   INFLOW   OUTFLOW TRAP EFF *
54.00  35.000 *   2.05     1.22    0.40 *
TOTAL= 33.000 *   2.05     1.22    0.40 *
*****
TIME   ENTRY *   SAND *
DAYS   POINT *   INFLOW   OUTFLOW TRAP EFF *
54.00  33.000 *   1.22     1.00    0.00 *
      15.000 *   1.00     0.00    0.00 *
TOTAL= 1.000 *   2.22     4.07   -0.83 *
*****
```

TABLE SB-1: SEDIMENT LOAD PASSING THE BOUNDARIES OF STREAM SEGMENT # 1

| SEDIMENT INFLOW at the Upstream Boundary: |                 |                    |                 |
|---|-----------------|--------------------|-----------------|
| GRAIN SIZE                                | LOAD (tons/day) | GRAIN SIZE         | LOAD (tons/day) |
| VERY FINE SAND...                         | 38.08           | VERY FINE GRAVEL.. | 0.00            |
| FINE SAND.....                            | 34.16           | FINE GRAVEL.....   | 0.00            |
| MEDIUM SAND.....                          | 21.06           | MEDIUM GRAVEL....  | 0.00            |
| COARSE SAND.....                          | 2.35            | COARSE GRAVEL....  | 0.00            |
| VERY COARSE SAND..                        | 0.61            | VERY COARSE GRAVEL | 0.00            |
| -----                                     |                 | -----              |                 |
|   |                 | TOTAL =            | 96.26           |

| SEDIMENT OUTFLOW from the Downstream Boundary |                 |                      |                 |
|---|-----------------|----------------------|-----------------|
| GRAIN SIZE                                    | LOAD (tons/day) | GRAIN SIZE           | LOAD (tons/day) |
| VERY FINE SAND. . . .                         | 115. 42         | VERY FINE GRAVEL. .  | 3. 19           |
| FINE SAND. . . . .                            | 101. 72         | FINE GRAVEL. . . . . | 3. 74           |
| MEDIUM SAND. . . . .                          | 348. 91         | MEDIUM GRAVEL. . . . | 1. 25           |
| COARSE SAND. . . . .                          | 332. 83         | COARSE GRAVEL. . . . | 0. 10           |
| VERY COARSE SAND. .                           | 108. 39         | VERY COARSE GRAVEL   | 0. 00           |
| -----   |                 | -----                |                 |
|   |                 | TOTAL =              | 1015. 54        |

TABLE SB-2: STATUS OF THE BED PROFILE AT TIME = 54.000 DAYS

| SECTION NUMBER | BED CHANGE (ft) | WS ELEV (ft) | THALWEG (ft) | Q (cfs) | TRANSPORT RATE (tons/day) SAND |
|----------------|-----------------|--------------|--------------|---------|--------------------------------|
| 58.000         | -2.93           | 976.06       | 972.47       | 532.    | 195.                           |
| 55.000         | -1.23           | 975.95       | 971.67       | 532.    | 193.                           |
| 53.000         | -1.54           | 974.32       | 970.66       | 660.    | 156.                           |
| 44.000         | 0.01            | 974.07       | 968.04       | 660.    | 7.                             |
| 42.000         | 0.00            | 974.02       | 970.00       | 689.    | 0.                             |
| 35.000         | 0.00            | 974.00       | 963.30       | 689.    | 0.                             |
| 33.900         | 0.22            | 964.63       | 962.87       | 689.    | 2576.                          |
| 33.300         | 0.03            | 963.41       | 962.52       | 689.    | 2295.                          |
| 33.000         | 0.00            | 963.00       | 961.00       | 689.    | 2295.                          |
| 32.100         | -0.31           | 961.87       | 956.19       | 689.    | 85.                            |
| 32.000         | -0.07           | 961.21       | 956.43       | 689.    | 241.                           |
| 15.000         | -0.23           | 957.71       | 953.47       | 750.    | 1016.                          |
| 1.000          | 0.00            | 957.00       | 944.70       | 750.    | 1016.                          |

Accumulated Water Discharge from day zero (sfd)

MAIN  
3500.00

SVOL A

STREAM SEGMENT # 1: EXAMPLE PROBLEM NO 4. SOME SEDIMENT OPTIONS.

SUMMARY TABLE: MASS AND VOLUME OF SEDIMENT

| SECTION | SEDIMENT THROUGH SECTION (tons) |         |      |      | SEDIMENT DEPOSITED IN REACH in cu. yds |            |         |      |      |
|---------|---------------------------------|---------|------|------|--|------------|---------|------|------|
|         | TOTAL                           | SAND    | SILT | CLAY | TOTAL                                  | CUMULATIVE | SAND    | SILT | CLAY |
| INFLOW  | 26932.                          | 26932.  | 0.   | 0.   | 21451.                                 |            |         |      |      |
| 58.000  | 34630.                          | 34630.  | 0.   | 0.   | -6132.                                 | -6132.     | -6132.  | 0.   | 0.   |
| 55.000  | 47052.                          | 47052.  | 0.   | 0.   | -9894.                                 | -16025.    | -9894.  | 0.   | 0.   |
| LOCAL   | 32721.                          | 32721.  | 0.   | 0.   | 26062.                                 |            |         |      |      |
| 53.000  | 104248.                         | 104248. | 0.   | 0.   | -19495.                                | -35520.    | -19495. | 0.   | 0.   |
| 44.000  | 73173.                          | 73173.  | 0.   | 0.   | 24751.                                 | -10769.    | 24751.  | 0.   | 0.   |
| LOCAL   | 733.                            | 733.    | 0.   | 0.   | 583.                                   |            |         |      |      |
| 42.000  | 4159.                           | 4159.   | 0.   | 0.   | 55553.                                 | 44784.     | 55553.  | 0.   | 0.   |
| 35.000  | 4159.                           | 4159.   | 0.   | 0.   | 0.                                     | 44784.     | 0.      | 0.   | 0.   |
| 33.900  | 2940.                           | 2940.   | 0.   | 0.   | 971.                                   | 45755.     | 971.    | 0.   | 0.   |
| 33.300  | 2475.                           | 2475.   | 0.   | 0.   | 370.                                   | 46125.     | 370.    | 0.   | 0.   |
| 33.000  | 2475.                           | 2475.   | 0.   | 0.   | 0.                                     | 46125.     | 0.      | 0.   | 0.   |
| 32.100  | 5577.                           | 5577.   | 0.   | 0.   | -2471.                                 | 43655.     | -2471.  | 0.   | 0.   |
| 32.000  | 7299.                           | 7299.   | 0.   | 0.   | -1371.                                 | 42283.     | -1371.  | 0.   | 0.   |
| LOCAL   | 2027.                           | 2027.   | 0.   | 0.   | 1615.                                  |            |         |      |      |
| 15.000  | 8242.                           | 8242.   | 0.   | 0.   | 863.                                   | 43147.     | 863.    | 0.   | 0.   |
| 1.000   | 8242.                           | 8242.   | 0.   | 0.   | 0.                                     | 43147.     | 0.      | 0.   | 0.   |

TOTAL SEDIMENT - per grain size - THROUGH EACH CROSS SECTION (tons)

|                 |        |         |      |         |    |
|-----------------|--------|---------|------|---------|----|
| UPSTREAM INFLOW |        |         |      |         |    |
| VF SAND         | 13463. | VC SAND | 122. | C GRVL  | 0. |
| F SAND          | 8809.  | VF GRVL | 0.   | VC GRVL | 0. |
| M SAND          | 4222.  | F GRVL  | 0.   |         | 0. |
| C SAND          | 316.   |         |      |         |    |
| LOCAL INFLOW    |        |         |      |         |    |
| VF SAND         | 2765.  | VC SAND | 0.   | C GRVL  | 0. |
| F SAND          | 6123.  | VF GRVL | 0.   | VC GRVL | 0. |
| M SAND          | 17758. | F GRVL  | 0.   |         | 0. |
| C SAND          | 6075.  |         |      |         |    |
| LOCAL INFLOW    |        |         |      |         |    |
| VF SAND         | 346.   | VC SAND | 11.  | C GRVL  | 0. |
| F SAND          | 214.   | VF GRVL | 4.   | VC GRVL | 0. |
| M SAND          | 122.   | F GRVL  | 2.   |         | 0. |
| C SAND          | 34.    |         |      |         |    |
| LOCAL INFLOW    |        |         |      |         |    |
| VF SAND         | 367.   | VC SAND | 55.  | C GRVL  | 0. |
| F SAND          | 732.   | VF GRVL | 24.  | VC GRVL | 0. |
| M SAND          | 709.   | F GRVL  | 10.  |         | 0. |

|             |        |         |      |         |    |
|-------------|--------|---------|------|---------|----|
| C SAND      | 129.   |         |      |         |    |
| SECTION NO. | 15.000 |         |      |         |    |
| VF SAND     | 320.   | VC SAND | 851. | C GRVL  | 3. |
| F SAND      | 1079.  | VF GRVL | 13.  | VC GRVL | 0. |
| M SAND      | 3214.  | F GRVL  | 14.  |         | 0. |
| C SAND      | 2742.  |         |      |         |    |
| SECTION NO. | 1.000  |         |      |         |    |
| VF SAND     | 320.   | VC SAND | 851. | C GRVL  | 3. |
| F SAND      | 1079.  | VF GRVL | 13.  | VC GRVL | 0. |
| M SAND      | 3214.  | F GRVL  | 14.  |         | 0. |
| C SAND      | 2742.  |         |      |         |    |

-----  
 SSEND

0 DATA ERRORS DETECTED.

TOTAL NO. OF TIME STEPS READ = 4  
 TOTAL NO. OF WS PROFILES = 23  
 ITERATIONS IN EXNER EQ = 1150

COMPUTATIONS COMPLETED  
 RUN TIME = 0 HOURS, 0 MINUTES & 9.00 SECONDS